



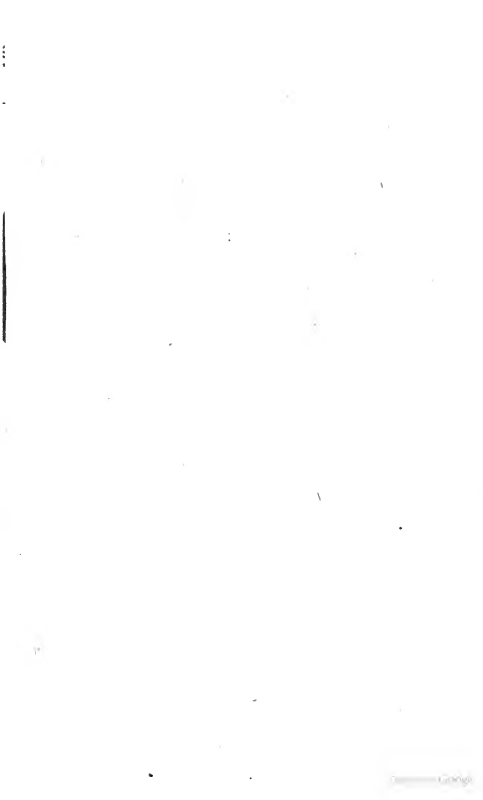
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THE
Elements of the Ellipse,
TOGETHER WITH
THE RADII OF CURVATURE,
&c.
RELATING TO THAT CURVE;
AND OF
CENTRIPETAL AND GENTRIFUGAL FORCES
IN
ELLIPTICAL ORBITS;

TO WHICH IS ADDED,
THE FIRST OF DR. MATTHEW STEWART'S
Tracts.

By JAMES ADAMS,



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THE
ELEMENTS OF THE ELLIPSE,
TOGETHER WITH
THE RADII OF CURVATURE,
&c.



P R E F A C E.

AT a time when Geometry is at its zenith, there doubtless appears but little occasion for a publication on the Conic Sections; and I therefore beg to offer the following reasons as an apology for my now presenting a Treatise on this subject to the public.

Having devoted the little leisure afforded me by an active employment, to the consideration of the Nature and Properties of the Radii of Curvature, &c. relative to the Conic Sections, I found that the generality of authors had confined themselves to the demonstration of the first principles.

It appeared to me also, that the Demonstrations of Hamilton, T. Newton, Robertson, and others, were too abstruse for learners; and that if a simple Definition of the Circle of Curvature were substituted in their place, a series of Propositions might be collected and arranged so as to render the study of this portion of Geometry more pleasing and less laborious.

In making this collection and arrangement, however, I perceived that there would be occasion to refer to more than one treatise on the Conic Sections, and I consequently resolved to select from the before mentioned, and a few other authors, some of the most useful properties of the Ellipse.

As any property of the Curve may be assumed as a Definition, I have chosen that which is used by the Rev. T.

Newton in his excellent little treatise on the Conic Sections.

The Proposition in which the Ellipse is formed by a plane cutting a cone, is placed near the commencement, (it being the 4th), in order to compare it with that which immediately precedes it, and thereby establish the validity of the first Definition.

It here occurred to me, that some observations on the Centripetal and Centrifugal forces, in relation to Elliptical Orbits, might be usefully introduced, and I accordingly selected a few Propositions for their elucidation.

The utility of the first of Dr. Matthew Stewart's Tracts in reference to the foregoing subjects, together with its scarcity, has induced me to republish it at the end of this work.

A variety of useful Propositions may in a similar manner be deduced from the Hyperbola and Parabola.

*Stonehouse,
near Plymouth.*

TO
THOMAS BEWES, ESQ.

THIS
Treatise
IS INSCRIBED,

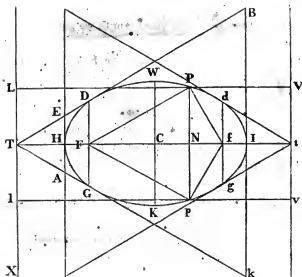
BY
HIS MUCH OBLIGED
AND
VERY HUMBLE SERVANT,
THE AUTHOR.



THE ELEMENTS OF THE ELLIPSE.

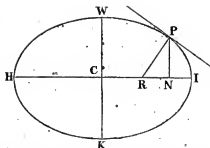
OF THE ELLIPSE.

DEFINITIONS.



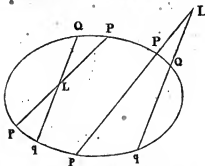
1. If any point F , be assumed without the line LX , and whilst the line FP revolves about F , as a center, a point P , moves in it in such a manner, that its distance from F , shall always be to PL (at right angles to LX) in a *given ratio*, the curve described by the point P , is called an *Ellipse*, FP being less than PL . See Proposition IV.

2. The line LX, is called the *Directrix*.
3. The point F, is called the *Focus*.
4. The line HI, drawn through the focus perpendicular to the directrix, is called the *Axis*.
5. The points H and I, where the curve meets the axis, are called the *Vertices*.
6. The line DFG, drawn through the focus parallel to the directrix, is called the *Principal Parameter*, or *Latus-rectum*.
7. The tangents TDB, TGK, which are drawn through the extremities of the latus-rectum, are called *Focal Tangents*.
8. The right line HI, is called the *Transverse Axis*, or *Axis Major*.
9. If the transverse axis be bisected in C, the point C, is called the *Center*.
10. If KW, which is bisected in C, be drawn perpendicular to HI, and $CW^2 = CK^2 = HF \times FI$; KW is called the *Conjugate Axis*, or *Axis Minor*.
11. A right-line PNp, drawn parallel to the tangent AHE, or perpendicular to HI, is called an *Ordinate to the Axis*.
12. The segments IN, NH, are called *Abscissas*.
13. Any line passing through the center, and terminated by the curve, is called a *Diameter*.
14. The points where the diameter meets the curve, are called the *Vertices* of that diameter.
15. If a right line be drawn from any point in a diameter parallel to the tangent at its vertex and terminated by the curve, it is called an *Ordinate* to that *Diameter*.
16. The segments of any diameter, between the ordinates and vertices, are called *Abscissas*.
17. A diameter, which is parallel to the tangent at the vertex of any diameter, is called a *Conjugate Diameter*.
18. A line, which is a third proportional to any diameter and its conjugate, is called a *Parameter* of that *Diameter*.



19. The right line PR, drawn perpendicular to the tangent, and intersecting the axis in R, is called a *Normal*.

20. The segment NR, is called a *Subnormal*.



DEF. 31. Right lines LPp, LQq, each meeting the section in two points, are called *Secants*; and L, the point of intersection, is called the *Point of Concourse*.

COROLLARY 1. (*Fig. page 1.*)

When the revolving line FP, comes into the position FHT; FP, PL, will become FH, HT; therefore $FH : HT :: FP : PL$.

COR. 2. When FP comes into the position of FD; FP, PL, will become FD, FT; therefore $FD : FT :: FP : PL$. Hence the latus-rectum DG is bisected in F.

COR. 3. The Ellipse has two foci and two directrices. For if

in HI produced, If be made equal to HF , and It to HT , and Vtv be drawn at right angles to HI , or parallel to LTl , and if fP revolve about f , in such manner, that fP, PV , have always the same *given ratio*, as FP, PL ; a curve would be described by the point P , similar and equal to that described by P , by the revolution of the line FP about the focus F . Therefore (Def. 2 and 3) Vtv is another directrix, and f another focus.

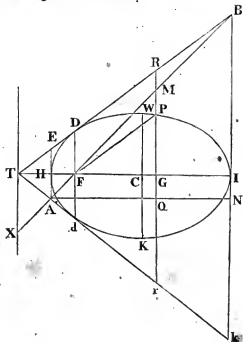
COR. 4. Since $HC=HI$ (def. 9) and $FH=fI$ (cor. 3), it follows that $CF=Cf$, and $CT=Ct$.

COR. 5. $CF+CI=Cf+CH=Hf=IF$.

COR. 6. $IF \times HF = Hf \times fI = CK^2 = CW^2$ (def. 10).

PROPOSITION I.

If TED , $TA d$ be focal tangents and a right line be drawn from any point P to the focus F , and the perpendicular RGP , meeting the tangent in R . Then $PF=RG$.



For the triangles TGR , TFD are similar.

Ther. $GR : GT :: FD : FT :: FP : GT$ (cor. 2. def.)

Hence $PF = RG$.

COR. If HE be drawn parallel to the directrix, then $HF = HE$. This is plain from the proposition.

PROP. II.

If from A where EH meets the tangent Td , a straight line be drawn through A and F , it will meet the tangent TD somewhere in B .

Produce FA to X . Then, because the triangles FHA , FTX are similar, and $FH = HA$ (cor. prop. 1.) $FT = TX$; but FD is less than FT (def. 1.) Ther. FD is less than TX , consequently the lines TD , XF must meet when produced.

COR. 1. If AF meet RG in M , then $FG = GM$. Because the triangles FGM , FHA are similar, and $FH = HA$; $FG = GM$.

COR. 2. When R coincides with B , then $RG = BI = FI$; but FP will become equal to FI (Prop. I.) Therefore the curve will meet the axis in I .

PROP. III.

The rectangle under the abscissæ, is to the square of the semi-ordinate to the axis, as the square of the transverse axis is to the square of the conjugate axis.

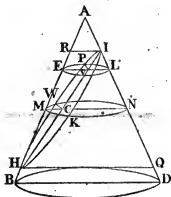
Draw AN parallel to HI ; then on account of the parallels, EHA , $RG r$, $BI k$, RM : $EA :: BM : BA :: QN : AN :: GI : HI$; and $Mr : Bk :: AM : AB :: AQ : AN :: HG : HI$. Therefore $RM \times Mr : EA \times Bk :: GI \times HG : HI^2$; but (5. 2. c) $RM \times Mr + MG^2 = RG^2 = FP^2$ and $MG^2 = FG^2$ (cor. 1. prop. 2.) ther. $RM \times Mr + FG^2 = FP^2$; ther. $RM \times Mr = PG^2$. $AE = 2HF$; $Bk = 2FI$; and (per def. 10.) $HF \times FI = CW^2$; hence by substitution $PG^2 : 4CW^2 :: HG \times GI : HI^2$; that is, $HG \times GI : PG^2 :: HI^2 : KW^2$.

COR. 1. Because HI and KW , are bisected in C ; $HG \times GI : PG^2 :: CI^2 : CK^2$.

COR. 2. The axis being constant; PG^2 varies as $HG \times GL$.

COR. 3. As the property is the same for the ordinates on both sides of the axis, at equal distances from the center, or from the vertices, the ordinates on both sides are equal; or the double ordinates are bisected by the axis.

PROP. IV.



If a cone ABD be cut through its two sides by a plane HW. PIK, the section will be an Ellipse.

Bisect HI in C, and let a section MWNK be drawn through C parallel to the base, and also another section EPLV parallel to MWNK; then will these sections be circles; hence, $EV \times VL = VP^2$, and $MC \times CN = CW^2$. Draw HQ, RI parallel to MN or EL;

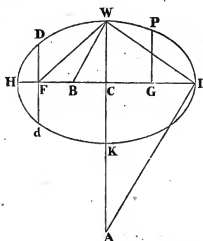
Then by similar triangles, $HC : CM :: HV : VE$; and $IC : CN :: IV : VL$.

Therefore $HC \times CI : CM \times CN :: HV \times VI : VE \times VL$.

That is $CI^2 : CW^2 :: HV \times VI : VP^2$; which is the property of the Ellipse by Prop. 3. Hence, according to Def. 1, the Ellipse is a conic section.

PROP. V.

The latus-rectum is a third proportional to the transverse and conjugate axes.



For $HC^2 : CK^2 :: HF \times FI : FD^2$ (Cor. 1. Prop. III.)

But $HF \times FI = CK^2$ (def. 10.) ther. $HC^2 : CK^2 :: CK^2 : FD^2$,

Or $HC : CK :: CK : FD$.

Cor. 1. $HG \times GI : GP^2 :: HI : \text{latus-rectum}$.

For $HI : KW :: KW : Dd$; or $HI : KW^2 :: 1 : Dd$; ther. $HI^2 : KW^2 :: HI : Dd :: HG \times GI : PG^2$.

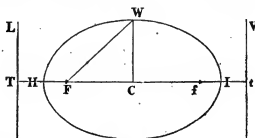
Cor. 2. If IW be joined, and WB and IA , be drawn at right angles thereto, intersecting the axes in B and A , then CB will represent the semi-parameter of the transverse axis, and CA , the semi-parameter of the conjugate axis. For from the nature of the right-angled triangles BIW and AIW ; $CB = \frac{CW^2}{CI}$,

and $CA = \frac{CI^2}{CW}$.

join CQ . Then because $CN=CG$; $QN=PG$ (Cor. 3. Prop. III.) and the angles at G and N are right angles, the triangles CNQ , CGP are equal. Ther. $CQ=CP$; and the angles NCQ , GCP being equal, PCQ is a straight line bisected in C .

PROP. IX.

If HI be the transverse, and CW the semi-conjugate axis, C the center, Ff the foci, and LT , Vt the directrices; then $HI : Tt :: HF : HT$.



For $FH : HT :: FI : IT$ (def. 1.)

Ther. $FH + FI : HT + IT :: HF : HT$.

That is, $HI : Tt :: HF : HT$.

COR. 1. Since Tt and HI are bisected in C ; $CH : CT :: HF : HT$.

COR. 2. $CF : CH :: HF : HT$.

For $FI : IT :: FH : HT :: fI : HT$; ther. $FI - fI : IT - HT :: fI : HT$.

That is, $Ff : HI :: fI : HT$; or $CF : CH :: HF : HT$.

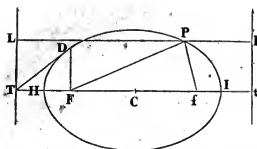
COR. 3. $CF : CH :: CH : CT$.

For $HI : Tt :: HF : HT$; or $CH : CT :: HF : HT$; ther. by cor. 2. $CF : CH :: CH : CT$.

COR. 4. Since $CF \times (CF + FT) = CH^2 = CF^2 + CW^2$ (Prop. VI.) or, $CF^2 + CF \times FT = CF^2 + CW^2$; it follows $CF \times FT = CW^2$.

PROP. X.

If from any points in the curve, two right lines be drawn to the foci, their sum is equal to the transverse axis.



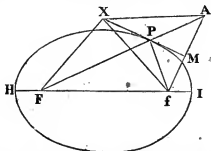
Let HI be the transverse axis, and F, f , the foci, and TL, tl , the directrices; from any point P , draw PF, Pf , and through P , draw LP parallel to HI ; then will Ll be equal to Tt .

By def. 1. and cor. 2 and 3. prop. IX. $PF : PL :: CF : CH :: CH : CT :: 2CH : 2CT :: HI : Tt$. But as $PF : Pf :: PL : Pl$; we have $PF + Pf : PF :: PL + Pl : PL$; that is, $PF + Pf : Tt :: PF : PL$;

Ther. $HI : Tt :: PF + Pf : Tt$; consequently $PF + Pf = HI$.

PROP. XI.

If from any point P in the curve, PF, Pf be drawn to the foci; the line PM , bisecting the angle fPA , will touch the curve in the point P .



Produce FP to A , so that PA equal Pf , and let a point X be taken in the line PM , and draw XF, Xf, XA , and also fA meeting PM in M . Then because in the triangles PMf, PMA ; $Pf = PA$ and PM common to both, and the angles MPA, MPf

equal; $Mf=MA$, and the angles at M right angles; therefore $Xf=XA$; but $XF+XA$ are greater than FA , that is, than $FP+PF$ or HI (Prop. X.), therefore the point X is not in the curve, and consequently the line PM touches the curve in the point P .

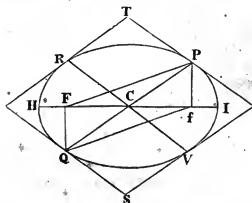
COR. 1. If from any point P in the curve two right lines be drawn to the foci, they will make equal angles with the curve, or with the tangent drawn through the point P .

For the $\angle APM=FPX$, ther. the $\angle fPM=FPX$.

COR. 2. If from the focus f , fM be drawn at right angles to the tangent PM , and intersect FP produced in A , then FA will be equal to the transverse axis HI . For $PA=Pf$, and (Prop. X.) $FP+Pf=FP+PA=FA=HI$.

PROP. XII.

The tangents at the vertices of any diameter are parallel.



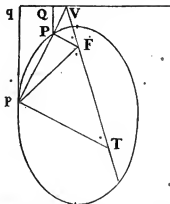
Let PCQ be any diameter, HI the transverse axis, F, f , the foci, and C the center. Draw the tangents PT, QS ; FP, Pf , fQ and QF . Then because $FC=Cf$ (cor. 4. def.) and $CP=CQ$ (Prop. VIII.) also the $\angle PCf=fCQ$, and $\angle FCP=fCQ$, it follows that FP is equal and parallel to Qf ; and FQ equal and parallel to Pf ; ther. $FPfQ$ is a parallelogram, hence the

$\angle F P f = F Q f$, and the halves of their supplements will be equal (Cor. Prop. XI.) that is, the $\angle F P T = f Q S$, to which add the equal angles $F P Q$, $f Q P$, and the $\angle Q P T = P Q S$; therefore $P T$ is parallel to $Q S$.

COR. If tangents be drawn at R and V , the vertices of any other diameter $R C V$, and produced to meet the tangents $P T$ and $Q S$, a parallelogram will be formed circumscribing the Ellipse.

PROP. XIII.

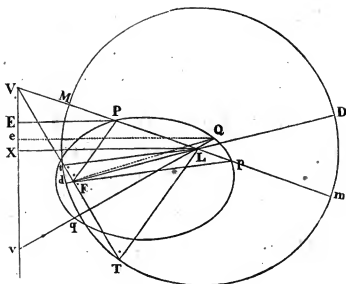
If a right line $P p$, which cuts the curve in P, p , meet the directrix in V , and a right line $V F T$ be drawn through the focus, and $F P$, $F p$ joined; then the $\angle P F V = \angle p F T$.



Draw $p T$ parallel to $P F$ to meet $v F$ in T ; and draw $P Q$, $p q$ perpendicular to the directrix. Then the triangles $V P Q$, $V p q$ are similar; as are also the triangles $V F P$, $V T p$. And $F P : P Q :: F p : p q$ (def. 1.) Or $F P : F p :: P Q : p q :: P V : p V :: P F : p T$, ther. $p T = p F$; and the angle $p F T = p T F$, which is equal to $P F V$ (by construction);

PROP. XIV.

If two right lines $P p$, $Q q$ intersect each other in L , and meet the directrix in V, v ; then $P L \times L p$ and $Q L \times L q$ will be in a constant ratio to each other, wherever L , the point of concourse be taken.



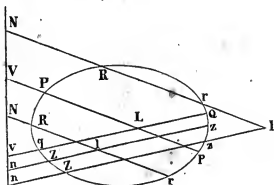
Let F be the nearest focus to the directrix Vv ; join VF and produce it, also join FP , Fp ; draw PE , LX perpendicular to the directrix; draw LT parallel to PF , and Lt parallel pF meeting VF in T and t .

$\angle PFV = \angle pFT$ (Prop. XIII.) ther. $\angle LTT = \angle LtT$; hence $LT = Lt$. From the center L , and distance LT or Lt , describe a circle, cutting VPp , in M and m ; join FL , and produce it to meet the circle in D and d . The triangles VPE and VLX are similar, as are also the triangles VPF , VLt . Ther. $LT : PF :: LV : PV :: LX : PE$; that is, $LT : LX :: FP : PE$, a given ratio (Prop. I.) Ther. $LT = \frac{FP}{PE} \times LX$; hence LT varies as LX . Because LT is parallel to PF , and Lt to pF ; $LP : TF :: LV : TV$, and $pL : Ft :: LV : tV$. Ther. $LP \times Lp : FT \times Ft :: LV^2 : VT \times Vt$. But $FT \times Ft = FD \times Fd$; and $VT \times Vt = Vm \times VM = VL^2 - ML^2$, ther. by substitution, $LP \times Lp : FD \times Fd :: VL^2 : VL^2 - ML^2$. But $LV :$

$LT(LM) :: PV : PF$, and $LV^2 : LM^2 :: PV^2 : PF^2$; ther.
 by division $LV^2 : LV^2 - LM^2 :: PV^2 : PV^2 - PF^2 :: LP \times Lp :$
 $FD \times Fd$. Per trig. $PV : PE :: \text{Rad.} : \sin. V$. whence $PV^2 =$
 $\frac{PE^2}{\sin.^2 \angle V}$ (radius 1.) $= \frac{PE^2}{s^2}$, ther. by sub. for PV^2 , we have
 $PL \times Lp : DF \times Fd :: \frac{PE^2}{s^2} : \frac{PE^2}{s^2} - PF^2 :: PE^2 : PE^2 - s^2 \times$
 $PF^2 :: 1 : 1 - \frac{PF^2}{PE^2} \times s^2 :: 1 : 1 - v^2 s^2$. That is, $PL \times Lp :$
 $FD \times Fd :: 1 : 1 - v^2 s^2$ ($v^2 = \frac{PF^2}{PE^2}$; and $s^2 = \sin.^2 LVX$.) In
 the same manner it may be proved that, $QL \times Lq : FD \times Fd ::$
 $1 : 1 - \frac{QF^2}{QE^2} \times \sin.^2 LvX$. That is, $QL \times Lq : FD \times Fd ::$
 $1 : 1 - v^2 r^2$; (by joining QF , drawing Qe perpendicular to VX ,
 and putting $r^2 = \sin.^2 LvX$.)

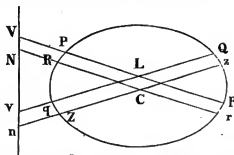
Hence $PL \times Lp : QL \times Lq :: 1 - v^2 r^2 : 1 - v^2 s^2$.

COR. 1. If any other two right lines Rr , Zz , intersect each
 other in l , (either within or without the curve), being respec-
 tively parallel to Pp , Qq , their rectangles will be in the same
 given ratio, that is, $PL \times Lp : QL \times Lq :: Rl \times lr : Zl \times lz$.

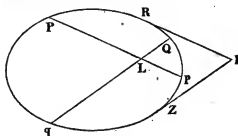


For the parallel lines make the angles at N and n with the
 directrix respectively equal to the angles at V and v .

Cor. 2. If the right lines Rr , Zz , which are respectively parallel to Pp , Qq ; intersect each other in the center C . Then $PL \times Lp : QL \times Lq :: CR^2 : CZ^2$. Because Rr , Zz ; make the same angles with the directrix, as Pp , Qq , and are each bisected in the center (Prop. VIII.) the corollary is manifest.

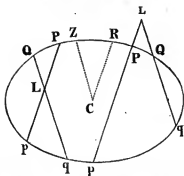


Cor. 3. If the lines Pp , Qq , move parallel to themselves until they touch the curve in R and Z , and meet in l ; then $PL \times Lp : QL \times Lq :: Rl^2 : Zl^2$. For when Pp touches the curve, P , and p will coincide in R , and $PL = Rl = pl$; ther. $PL \times Lp = Rl^2$. In like manner, $QL \times Lq = Zl^2$.

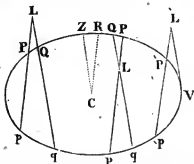


Cor. 4. If two right lines meeting each other, be respectively parallel to two diameters, according to their both touching, or both cutting, or one of them touching and the other cutting the curve, the squares of the segments of the tangents, or the rectangles under the segments of the secants, will be in a constant ratio to each other, wherever the point of concurrence be taken.

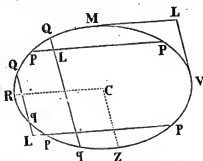
SCHOLIUM.



If four secants, intersecting each other, are respectively parallel to two semi-diameters; then $PL \times Lp : QL \times Lq :: CR^2 : CZ^2$

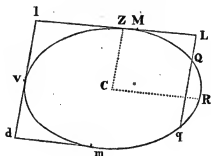


If three of the lines be secants, and one a tangent, then $PL \times Lp : QL \times Lq :: 'L'P \times 'L'p : 'L'V^2 :: CR^2 : CZ^2$.

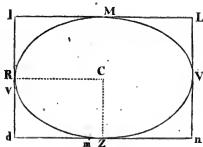


If two of the lines be secants and two tangents, then $PL \times Lp : QL \times Lq :: LM^2 : LV^2 :: CR^2 : CZ^2$.

If one of the lines is a secant and three tangents, then $dm^2 : dv^2 :: LM^2 : LQ \times Lq :: CR^2 : CZ^2$; $lM^2 : lv^2 :: LM^2 : LQ \times Lq :: CR^2 : CZ^2$. Ther. $dm : dv :: lM : lv$.

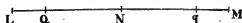


If the four lines be tangents, and touch the curve in M, V, m, v; then, $dm : dv :: lM : lv :: LM : LV :: nm : nV :: CR : CZ$.



LEMMA I.

If the straight line LM be so divided in Q and q that $LQ \times Lq = MQ \times Mq$; or $LQ \times QM = Mq \times qL$; then $LQ = Mq$.



First, bisect LM in N.

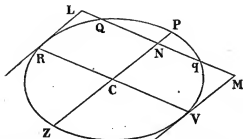
Then (5. 2. E.) $LQ \times QM + QN^2 = LN^2 = Mq \times qL + qN^2$.

But $LQ \times QM = Mq \times qL$; ther. $QN^2 = qN^2$; that is, $QN = Nq$. Ther. $LN - QN = MN - qN = LQ = Mq$.

Secondly, bisect Qq in N ; then (6. 2. E.) $Lq \times LQ + QN^2 = LN^2$, and $Mq \times Mq + qN^2 = MN^2$; but $LQ \times Lq = Mq \times Mq$, and $QN^2 = Nq^2$; ther. $LN^2 = MN^2$; that is, $LN = NM$. Hence $LN - QN = MN - qN = LQ = Mq$.

PROP. XV.

All right lines drawn parallel to any diameter, and which are terminated by the curve, are bisected by the conjugate diameter.



Let RCV be any diameter, and PCZ its conjugate; through the vertices R, V , draw the tangents RL, VM ; and through any point N in PZ , draw $LN M$ parallel to RV , meeting the curve in Q and q , and the tangents in L and M . On account of the parallel lines, $RL = VM$, and $LN = NM$; and (Cor. 4. Prop. XIV.) $RL^2 : MV^2 :: LQ \times Lq : MQ \times Mq$; ther. $LQ \times Lq = MQ \times Mq$; hence by the Lemma, $LQ = Mq$; ther. $LN - LQ = MN - Mq = QN = Nq$.

PROP. XVI.

If PCZ be any diameter, RCV its conjugate, and QN a semi-ordinate. Then $PN \times NZ : QN^2 :: CZ^2 : CV^2$.

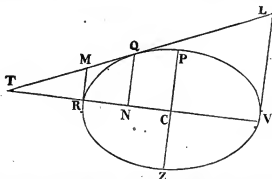
For (by Cor. 4. Prop. XIV.) $PN \times NZ : QN \times Nq (=QN^2) :: CZ^2 : CV^2$.

Cor. 1. Since $PN \times NZ : QN^2 :: CZ^2 : CV^2 :: CZ : \frac{CV^2}{CZ} :: 2CZ : \frac{2CV^2}{CZ}$; ther. $PN \times NZ : QN^2 :: PZ : \text{Param. of } PZ$ (def. 18.).

COR. 2. CZ and CV being constant, $PN \times NZ$ will vary as QN^2 .

PROP. XVII.

If QT be a tangent at any point Q , and meet the diameter VR in T ; and QN be a semi-ordinate, then $CN : CR :: CR : CT$.



Draw the tangents RM , VL to meet the tangent QT in M and L .

Then (Cor. 4. Prop. XIV. and the parallel lines RM , NQ and VL) $MQ : QL :: MR : LV :: RT : VT :: RN : NV$; by division, $VT - RT : RT :: NV - RN : RN$; that is, $RV : RT :: NC + CR - RN : RN$.

Or, $RV : RT :: 2NC : RN$; or, $CR : RT :: NC : RN$; by composition, $CR + RT : CR :: CN + NR : CN$.

That is, $CT : CR :: CR : CN$; or, $CN : CR :: CR : CT$.

COR. 1. $RN : NC :: TN : NV$.

For $CN : CV :: CV : CT$; by composition, $CN + CV : CN :: CV + CT : CV$.

That is, $NV : NC :: VT : VC$; or, $CN : CR :: NV : VT$; by division, $CR - CN : CN :: VT - VN : VN$;

That is, $RN : NC :: TN : NV$.

COR. 2. $TR : TN :: TC : TV$.

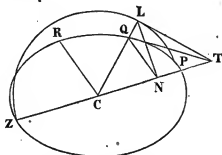
For $CT : CR :: CR : CN$; by division, $CT - CR : CT :: CR - CN : CR$.

That is, $TR : CT :: RN : CR$; by composition, $TR + RN : TR :: CT + CR : CT$.

Or, $TN : TR :: VT : TC$; $TR : TN :: TC : TV$.

PROP. XVIII.

If a circle ZLP be described on the diameter PZ , and NL be drawn perpendicular thereto, and NQ an ordinate to the curve; then, $NL : NQ :: CZ : CR$.

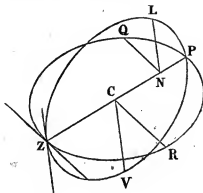


For, by Prop. XVI. $PN \times NZ : NQ^2 :: CZ^2 : CR^2$. And, by a property of the circle, $PN \times NZ = NL^2$; ther. $NL^2 : NQ^2 :: CZ^2 : CR^2$; that is, $NL : NQ :: CZ : CR$.

COR. CZ and CR being constant, CL will vary as NQ .

PROP. XIX.

If two Ellipses $ZLPV$, $ZQPR$, be described on the same diameter PZ , and the ordinates NL , NQ be drawn, and the semi-diameters CV , CR parallel to these ordinates be also drawn, then $NL : NQ :: CV : CR$.



By Prop. XVI. $PN \times NZ : NL^2 :: CP^2 : CV^2$.

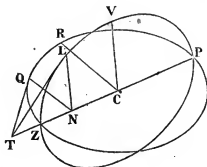
And, $PN \times NZ : NQ^2 :: CP^2 : CR^2$.

Therefore, $NL^2 : CV^2 :: NQ^2 : CR^2$.

That is, $NL : NQ :: CV : CR$.

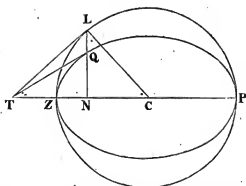
PROP. XX.

If $ZLVP$, $ZQRP$ be two Ellipses, having a common diameter, PZ ; NL , NQ ordinates thereto, and CV , CR semi-diameters parallel to these ordinates; tangents drawn at L and Q will intersect each other in T , a point in the diameter PZ , produced.



Since PZ is a common diameter to both curves, and the ordinates are drawn from the same point N , and by Prop. XVII. $CN : CZ :: CZ : CT$; then TL , TQ are tangents at the points L and Q .

COR. 1. If a circle ZLP , and an ellipse ZQP have a common diameter PZ and a common abscissa ZN ; tangents at the extremities of the ordinates NL , NQ will meet each other in T , a point in the diameter PZ , produced. Draw LT a tangent to the circle and join TQ , and CL ; then because the triangles CLT and CNL are similar, $CN : CL :: CL : CT$. Or, $CN : CZ :: CZ : CT$. Therefore TQ touches the ellipse in Q .

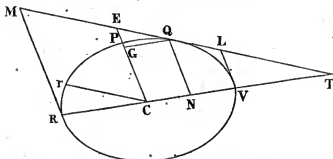


COR. 2. If one of the curves be a circle and the other an ellipse having the ordinates NL , NQ as in fig. to Prop. XVIII. tangents at L and Q , will meet each other in T , for the same reason as in Cor. 1.

PROP. XXI.

Draw through the extremities of any diameter RV , two tangents to meet any other tangent QM , in the points L, M ; and let CP be conjugate to RV and Cr parallel to LM .

Then $RM \times VL = CP^2$; and $MQ \times QL = Cr^2$.



CASE 1. Draw the ordinates QN , QG ; by Prop. XII. RM and VL are parallel, and by Prop. XVII. $CN \times CT = CV^2$. Therefore $CT^2 - CN \times CT = (CT - CN) \times CT = NT \times CT$. And $CT^2 - CV^2 = RT \times VT$; ther. $RT \times VT = NT \times CT$; Hence $RT : TN :: CT : VT :: CE : VL$ (sim. triangles). But $RT : NT :: RM : NQ$. Ther. $RM : NQ :: CE : VL$, ther. $RM \times VL = CE \times NQ = CE \times CG = CP^2$ (Prop. XVII.)

CASE 2. Because (Cor. 4. Prop. XIV.) $MR : MQ :: LV : LQ$; it will be $MR^2 : MR \times LV :: MQ^2 : MQ \times LQ$; by substitution, $MR^2 : CP^2 :: MQ^2 : MQ \times LQ$; but (Cor. 4. Prop. XIV.) $MR^2 : MQ^2 :: CP^2 : Cr^2$; ther. $CP^2 : Cr^2 :: CP^2 : MQ \times LQ$; ther. $MQ \times LQ = Cr^2$.

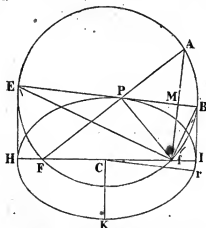
PROP. XXII.

If a tangent at any point Q, meet the transverse and conjugate diameters CV, CP, in T and E, and Cr be drawn parallel to TM, then $EQ \times QT = Cr^2$.

Draw the ordinate QN, and through the vertices of the diameter RV; draw the tangents RM, VL, which (Prop. XII.) are parallel to each other, as well as to the ordinate NQ; by Cor. I. Prop. XVII. $CN \times NT = RN \times NV$. Ther. $CN : NV :: RN : NT :: EQ : QL :: MQ : QT$ (sim. triang.) Hence $EQ \times QT = LQ \times QM = Cr^2$, (Prop. XXI.)

PROP. XXIII.

Draw through the extremities of the transverse axis HI, two tangents to meet any other tangent PM in the points E, B; then a circle described about EB as a diameter will pass through the foci F, f.



Let CK be the semi-conjugate axis, and join fB, fE, fP and FP, which last produce to A, and join fA which will intersect EB in M. Then (Def. 10. and Prop. XXI.) $Hf \times fI = HE \times$

$IB=CK^2$. Ther. $HE:Hf::lf:IB$. These lines are about the equal angles at H and I ; therefore the triangles HEf , IBf are equiangular, and the angles BfI , fEH equal; but $BfI+IBf=BfI+EfH=a$ right angle, therefore BfE is a right angle, and consequently the point f is in the circumference of the circle described about BE . In like manner it may be shewn that the other focus F is in the circumference of the same circle.

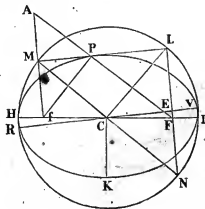
PROP. XXIV.

If PF , Pf , be drawn from any point P in the curve to the foci, and Cr parallel to the tangent EPB , then $PF \times Pf = Cr^2$.

Draw the tangents HE , IB ; then (Prop. XXIII.) a circle described about the diameter EB will pass through the foci. Draw from either focus as f , the perpendicular fM to EB , and let it meet FP in A ; and because the angles fPM , APM are equal (Prop. XI.) and PM common; $fM=MA$; and $Pf=PA$; therefore because the diameter EB of the circle bisects fA , and is perpendicular to it, and the point f is in the circumference, the point A will be in the same; therefore by a property of the circle $FP \times PA = FP \times Pf = EP \times PB = Cr^2$ (Prop. XXI.)

PROP. XXV.

If from the foci F , f ; FL , fM be drawn perpendicular to the tangent PM , a circle described about the transverse axis, will pass through the points L , M , where the perpendiculars meet the tangent.



Let HI be the transverse axis and C the center and join fP , FP ; let the perpendicular fM meet FP in A , and join CM . Because (Prop. XI.) the angles fPM , APM are equal and PM common, $fP=PA$ and thence, $FA=HI$ (Prop. X.) But $fM=MA$; and likewise $fC=CF$ (Cor. 4. Def.) ther. FA and CM are parallel, and thence $CM=\text{half } FA=\text{half } HI$. Therefore M is in the circumference of the circle described about HI ; and in like manner the point L will be in the same circumference.

COR. If the diameter RCV be parallel to the tangent PM , it will cut off from PF the segment PE , equal to half the transverse axis.

For $CMPE$ is a parallelogram, ther. $PE=CM=\text{half } HI$.

PROP. XXVI.

If the perpendiculars FL , fM be drawn from the foci F , f , to the tangent PM , then will $FL \times fM = CK^2$.

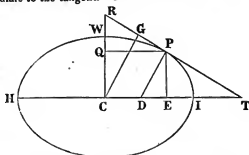
Let HI be the transverse and CK the semiconjugate axis, and C the center. Join CM , CL , and let CM meet FL in N . Because FN , fM are parallel, the triangles CfM , CFN are equiangular, and because $CF=Cf$ (Cor. 4. Def.); $CM=CN$, and $FN=fM$, $CM=CL=CN$; the point N , is therefore in the circumference of the circle described about the transverse axis HI as a diameter. Hence by a property of the circle $FL \times FN = FL \times fM = HF \times FI = CK^2$ (Def. 10.)

COR. 1. $FL^2 = \frac{FP}{fP} \times CK^2$. For the triangles FPL , fPM are similar, ther. $FP:FL::fP:fM$, or $FP \times fM = FL \times fP$, or $FP \times fM \times FL = FL^2 \times fP$. ther. $FL^2 = \frac{FP}{fP} \times fM \times FL = \frac{FP}{fP} \times CK^2$.

COR. 2. CK^2 being constant; FL^2 will vary as $\frac{FP}{fP}$.

PROP. XXVII.

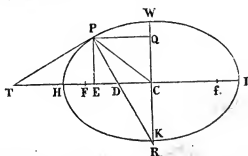
Let HI be the transverse and CW the semi-conjugate axis, C the center, and PT a tangent at P ; let PD and CG be perpendiculars to the tangent. Then $Pd \times CG = CW^2$.



Draw PE , PQ perpendicular to the axes, and let CW meet PT in R ; then $QC = PE$; and on account of the parallel lines, the right-angled triangles CGR and PED are similar, and $CG : CR :: PE : PD$, ther. $CG \times PD = CR \times PE = CR \times CQ = CW^2$ (Prop. XVII.)

PROP. XXVIII.

If PE be an ordinate to the transverse axis, and PD perpendicular to the tangent at P , and F, f , the foci; then $HI : \text{latus-rectum} :: CE : ED$.



For $CE : ED :: CE \times ET : ED \times ET$; but $CE \times ET = IE \times EH$ (Cor. 1. Prop. XVII.) And because DPT is a right angle, $ED \times ET = EP^2$, therefore $CE : ED :: IE \times EH : EP^2 :: HI : \text{latus-rectum}$. (Cor. 1. Prop. V.)

COR. 1. $CE:ED::CH^2:CW^2$. For $CE:ED::HI:KW^2$
 $\frac{KW^2}{HI}::HI^2:KW^2::CH^2:CW^2$.

COR. 2. $CE:CD::CH^2:CF^2$. For $CE-ED:CE::CH^2-CW^2:CH^2::CF^2:CH^2$; that is, $CE:CD::CH^2:CF^2$.

COR. 3. Produce PD to cut the conjugate axis WK in R, draw the ordinate PQ and join CP. Then $QR:QC::CH^2:CW^2$.

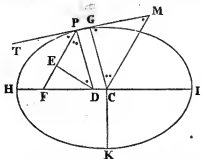
For by sim. triangles $QR:QP::PE:ED$; or $QR:QC::CE:ED::CH^2:CW^2$ (Cor. 1.)

COR. 4. $\text{Tang. EDP}:\text{Tang. ECP}::CI^2:CK^2$.

For $EC:ED::\text{Tang. EPC}:\text{Tang. EPD}::\text{Cotang. EPD}:\text{Cotang. EPC}::\text{Tang. EDP}:\text{Tang. ECP}$. That is, $EC:ED::\text{Tang. EDP}:\text{Tang. ECP}::CI^2:CK^2$.

PROP. XXIX.

If a right line DE be drawn from the point D, where the normal meets the transverse axis, perpendicular to the distance PF, between the point of contact and focus, it will cut off the segment PE equal to half the latus-rectum.

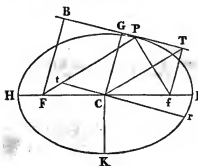


Draw CG perpendicular to PT and CM parallel to PF, and let CK be the conjugate semi-axis; then on account of the parallel lines, the right angled triangles CGM, DEP are equiangular, and $CM:CG::DP:PE$, ther. $CM \times PE = CG \times DP = CK^2$ (Prop. XXVII) But (Cor. Prop. XXV.) $CM = CI$,

Ther. $\frac{MF+FN}{MF \times FN} = \frac{HI}{HF \times FI} = \frac{HI}{CK^2}$ (Cor. 6. Def.) $= \frac{1}{FN}$
 $+ \frac{1}{FM} = \frac{2}{\text{latus-rectum}}$, CK being the semi-conjugate.

PROP. XXXI.

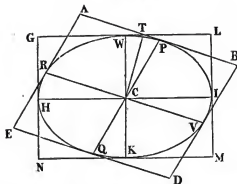
If HI be the transverse and CR CK the semi-conjugate axis, F, f, the foci, FB drawn perpendicular to the tangent PT, FP joined and Cr drawn parallel to PT, then $FB : FP :: CK : Cr$.



Draw fT perpendicular to PT and join fP; because the angles fPT, FPB are equal (Cor. Prop. XI.) the right angled triangles fTP, FBP are similar, and $FB : FP :: fT : fP$, or, $FB^2 : FB \times fT :: FP^2 : FP \times fP$, that is, $FB^2 : FP^2 :: CK^2 : Cr^2$. (Prop. XXIV. and XXVI.) Ther. $FB : FP :: CK : Cr$.

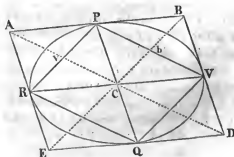
COR. 1. If from the center C, CG be drawn perpendicular to the tangent PT, then $CG \times Cr = CI \times CK$. For draw CT parallel to FP, then (Cor. Prop. XXV.) $CT = Pt = CI$, and the triangles GCT, BFP similar; ther. $CG : CT :: FB : FP :: CK : Cr$; that is, $CG : CI :: CK : Cr$; or, $CG \times Cr = CI \times CK$.

COR. 2. If a parallelogram ABDE be formed by drawing tangents through the vertices of any two conjugate diameters PQ, RV, it will be equal to the rectangle under the axes.



Let C be the center, HI , KW the axes, and RV , PQ the conjugate diameters; the tangents drawn through the vertices P V Q R will form a parallelogram. (Cor. Prop. XII.) Let the tangents drawn through P and V meet at B ; $PCVB$ will then be a fourth part of the parallelogram $ABDE$; draw CT perpendicular to AB or RV , then (Cor. 1.) $CT \times CV = CI \times CK$; that is, the parallelogram $PCVB = CIKM$; ther. $ABDE = GLMN$.

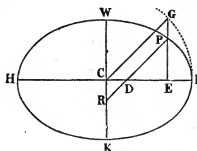
COR. 3. The inscribed parallelogram $QRPV$ is half the circumscribed parallelogram $ABDE$.



By drawing the diagonals AD , BE , it will plainly appear that $QRPV$ is a *parallelogram*, and that the parallelogram $PVCb$ is *half* the parallelogram $PCVB$, whence the Cor. is evident.

PROP. XXXII.

If HI be the transverse, KW the conjugate axis, and C the center, and if the difference between CI and CK be set from a point R in the conjugate to meet the transverse in D , and RD produced to P , so that DP be equal to CK , the point P will be in the ellipse.



Draw PE an ordinate to the transverse axis, and CG parallel to RD to meet EP in G ; because CR , PG are parallel, CG is equal to RP : that is (by construction) to CI ; therefore the point G is in the circumference of a circle described about HI ; and because the triangles PED , GEC are similar, $PE^2 : GE^2 :: PD^2 : GC^2$; that is, $PE^2 : HE \times EI :: CK^2 : CI^2$; therefore the point P is in the ellipse (Prop. XVI.)

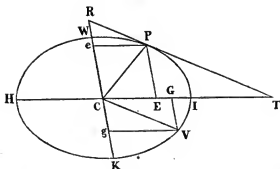
COR. If two right lines HI , KW bisect each other at right angles in the point C , and $RD = CI - CK$, and $DP = CK$; and the line RD be moved through four right angles, so that the point R be always in KW , and D in HI , the point P will describe an ellipse whose transverse axis is HI , and whose conjugate is KW .

Hence the construction of the *elliptical compass*, or *trammel* is evident.

PROP. XXXIII.

If CP , CV be two conjugate diameters, C the center, and the ordinates PE , VG be drawn to a third diameter HI ,

Then $HG \times GI = CE^2$; and $HE \times EI = CG^2$.



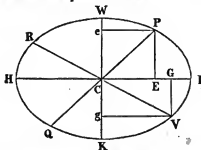
For draw the tangent PT meeting CW in R , then because PT is parallel to CV and PE to VG , the triangles PET , VGC are equiangular; and therefore $RP : PT :: CE : ET$. Or, $RP \times PT : CE \times ET :: PT^2 : ET^2 :: CV^2 : CG^2$; but (Prop. XXII.) $RP \times PT = CV^2$, therefore $CE \times ET = CG^2 = HE \times EI$ (Cor. 1. Prop. XVII.) $= CI^2 - CE^2$. And $CI^2 - CG^2 = HG \times GI = CI^2 - CI^2 + CE^2 = CE^2$.

Cor. 1. $CE^2 + CG^2 = CI^2$. For $CE^2 + CG^2 = HG \times GI + HE \times EI = CI^2$, $EI^2 - CG^2 + CI^2 - CE^2$; ther. $CE^2 + CG^2 = CI^2$.

Cor. 2. $EP^2 + GV^2 = CW^2$. For by drawing the ordinates Pe , Vg ; $Ce^2 + Cg^2 = EP^2 + GV^2 = CW^2$.

PROP. XXXIV.

The sum of the squares of any two conjugate diameters is equal to the sum of the squares of the axis.



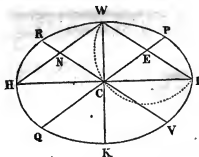
Let CI , CW be the semi-axes, and CP , CV two conjugate

Secondly. Let RCV be any diameter, and RGQ an ordinate to either axis, and join CQ . Then GR being equal to GQ , and CG common to the two right angled triangles CGR , CGQ , the triangles are equal; ther. $CQ=CR$, and the angle $QCG=RCG$.

COR. Hence if the semi-diameters CR , CQ be equal, and the angle RCQ bisected by the line CH , the position of the axis will be determined.

PROP. XXXVI.

The two diameters which bisect the right lines joining the vertices of the axes, are equal and conjugate diameters.



Let HI , KW be the axes; join IW , WH , and draw the diameters PQ , RV , bisecting the lines IW , WH , in E and N . Because IW , WH are bisected by the diameters PQ , RV , they are ordinates to these diameters. (Prop. XV.) And because HI is bisected in C , and IW in E , CE is parallel to HW ; therefore PQ , RV are conjugate diameters; and the angle ICW being a right angle, it will be in a semicircle, of which IW is the diameter, and E the center; therefore EI will be equal to EC , and the angle ECI equal to the angle EIC , which is equal to the alternate angle ICV ; and therefore the diameters PQ , RV are equal. (Prop. XXXV.)

But $CP^2 = \frac{m^2 n^2}{c^2(n^2 + x^2 m^2)}$; ($c = \cos. ECP$).

Ther. $CE^2 = \frac{m^2 n^2}{(1+x^2)(n^2+x^2 m^2)c^2} = \frac{m^2 n^2}{n^2+x^2 m^2}$; $(1+x^2)c^2 =$
 rad.² by substituting for x^2 , we have $CE^2 = \frac{m^2 n^2}{n^2 + \frac{T^2 n^4}{m^2}} =$
 $\frac{m^4 n^2}{m^2 n^2 + n^4} = \frac{m^4}{m^2 + T^2 n^2}$ Ther. $CE = PQ = \frac{CH^2}{\sqrt{CH^2 + T^2 \cdot CK^2}}$.

To find the Normal PR.

Per trig. $\sin. PRQ : PQ :: \text{Rad.} : PR$.

Or, $C : PQ :: 1 : PR = \frac{PQ}{C} = \frac{CH^2}{C\sqrt{CH^2 + T^2 \cdot CK^2}}$. ($C = \cos. EDP$).

To find the Normal PD.

By Cor. 1. Prop. XXVIII. we have $EC : ED :: CH^2 : OK^2$.

Ther. $ED^2 = \frac{CE^2 \times CK^4}{CH^4} = \frac{n^4}{m^4} \times CE^2$, and per trig. $C^2 :$
 $ED^2 :: 1 : PD^2 = \frac{ED^2}{C^2} = \frac{n^4}{C^2 m^4} \times CE^2 = \frac{n^4}{C^2 m^4} \times \frac{m^4}{m^2 + T^2 n^2} =$
 $\frac{n^4}{C^2(m^2 + T^2 n^2)} \therefore PD = \frac{CK^2}{C\sqrt{CH^2 + T^2 \cdot CK^2}}$.

To find the Ordinate PE.

Per trig. $\text{Rad.} : PD :: \sin. EDP : PE \therefore PE^2 = \sin.^2 EDP = PD^2$.

That is, $PE^2 = \frac{S^2 \cdot n^4}{C^2(m^2 + T^2 n^2)} = \frac{T^2 n^4}{m^2 + T^2 n^2} = \frac{n^4}{n^2 + \frac{m^2}{T^2}} =$

$\frac{n^4}{n^2 + T^2 m^2}$.

Ther. $PE = \frac{CK^2}{\sqrt{CK^2 + T^2 \cdot CH^2}}$; ($S = \sin.$ and $T = \cot. EDP$).

To find the Distance CD.

By Cor. 1. Prop. XXVIII. we have $EC : ED :: CH^2 : CK^2$.

Ther. $EC - ED : EC :: CH^2 - CK^2 : CH^2 \therefore CD = \frac{CE}{CH^2} (CH^2 - CK^2)$.

That is, $CD = \frac{CH^2 - CK^2}{\sqrt{CH^2 - T^2} \cdot CK^2}$.

PROP. XXXVIII.

If the ellipse be nearly a circle, to find the variation of CP.

$$\begin{aligned} \text{By Prop. XXXVII. } CP^2 &= \frac{m^2 n^2}{c^2(n^2 + t^2 m^2)} = \frac{m^2 n^2}{c^2 n^2 + s^2 m^2} \\ &= \frac{m^2 n^2}{(1 - s^2)n^2 + s^2 m^2} = \frac{m^2 n^2}{n^2 - n^2 s^2 + m^2 s^2} = \frac{m^2 n^2}{n^2 + (m^2 - n^2)s^2} \\ &= \frac{m^2 n^2}{n^2 + (m + n)(m - n)s^2} = \frac{m^2 n^2}{n^2 + 2n(m - n)s^2} \text{ nearly,} \\ &= \frac{m^2 n^2}{\{n + (m - n)s^2\}^2} \text{ nearly,} \end{aligned}$$

Therefore $CP = \frac{mn}{n + (m - n)s^2}$ nearly.

From hence $m - CP = \frac{CP}{n} (m - n)s^2 = (m - n)s^2$ nearly,

And by substituting $1 - c^2$ for s^2 we have $CP - n = (m - n)c^2$ nearly; and by restoring the values of m, n, s and c , we obtain,

$\left. \begin{aligned} CH - CP &= (CH - CK) \times \sin^2 ECP \\ CP - CK &= (CH - CK) \times \cos^2 ECP \end{aligned} \right\} \text{ But } CH - CK \text{ is given, therefore}$
 $CH - CP$ is as $\sin^2 ECP$; and $CP - CK$ is as $\cos^2 ECP$ nearly.

COR. Since $CP - CK : CH - CP :: \cos^2 ECP : \sin^2 ECP$
 $\therefore 1 : \frac{\sin^2}{\cos^2} ECP :: 1 : \tan^2 ECP$ (rad. = 1).

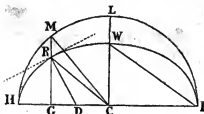
$$\begin{aligned} * CP &= \frac{mn}{\sqrt{n^2 + (m^2 - n^2)s^2}} = \frac{mn}{n + \frac{(m^2 - n^2)s^2}{2n}} \text{ nearly,} = \frac{2mn^2}{2n^2 + (m + n)(m - n)s^2} \\ &= \frac{2mn^2}{2n^2 + 2n(m - n)s^2} = \frac{mn}{n + (m - n)s^2}, \text{ as before.} \end{aligned}$$

the sum of the tangent and co-tangent of any angle will be the least possible, or $T + \frac{1}{T} = \frac{1+T^2}{T} = (1+T^2) \times \frac{1}{T} = \frac{1}{\cos.^2} \times \frac{\cos.}{\sin.}$
 $= \frac{1}{\sin. \times \cos. GCM} = \text{min.}$ Therefore $T + \frac{1}{T}$ is the least, when the $\sin. \times \cos.$ is the greatest, that is, when the $\sin. = \cos.$, or the angle GCM forty-five degrees, in which case $T=1$, therefore the tang. = cotang. Hence $\frac{CI}{T} = CW \times T$, ther. $T^2 = \frac{CI}{CW} = \text{tang. } CWI$, (by joining IW), and by substitution we have $\frac{(CI-CW) \times T}{CI+CW \cdot T^2} = \frac{CI-CW}{2CI \times CW} \times \sqrt{CI \times CW} = \text{tang. } RCM$ when a maximum.

If the ellipse do not differ much from a circle, (as is the case with our earth) the tang. RCM would be very nearly equal to $\frac{CI-CW}{2CI} = \frac{WL}{HI} = \frac{\text{diff. of semi-diam.}}{\text{transverse axis}}$ when a maximum. Or by making $T=1$, we obtain tang. $RCM = \frac{CI-CW}{CI+CW} = \frac{WL}{HI}$ nearly.

PROP. XL.

Let the figure in the margin be similar to that of Prop. XXXIX, and draw the normal RD , it is required to find the angle DRC , the difference between GRC and GRD .



Per Cor. 4. Prop. XXVIII. we have $GC : GD :: \text{tang. } GRC : \text{tang. } GRD :: CI^2 : CW^2$. Ther. $\text{tang. } GRC \times CW^2 = \text{tang. } GRD \times CI^2$. Put tang. $GRC = X$, and tang. $GRD = Y$; then

$$X = \frac{CI^2}{CW^2} \times Y. \text{ And per trig. } \left(\frac{CI^2}{CW^2} \times Y - Y \right) \div \left(1 + \frac{CI^2}{CW^2} \right) \\ = \text{tang. DRC} = \frac{(CI^2 - CW^2) \times Y}{CW^2 + CI^2 \cdot Y^2}. \text{ But tang. GRD} = Y = \\ \frac{CW^2}{CI^2} \times \text{tang. GRC} = \frac{CW^2}{CI^2} \times \text{cotang. GCR. But (Prop. XXXVIII.)} \\ \text{cot. GCR} = \frac{1}{T} = \frac{CI}{CW} \times \frac{1}{T} (T = \text{tang. GCM}).$$

$$\text{Therefore } Y = \frac{CW^2}{CI^2} \times \frac{CI}{CW} \times \frac{1}{T} = \frac{CW}{CI} \times \frac{1}{T}; \\ \text{and by substituting for } Y \text{ and } Y^2 \text{ we have tang. DRC} = \\ \frac{(CI^2 - CW^2) \times \frac{CW}{CI} \times \frac{1}{T}}{CW^2 + CI^2 \times \left(\frac{CW}{CI} \times \frac{1}{T} \right)^2} = \frac{CI^2 - CW^2}{CI \times CW} \times \frac{T}{1 + T^2} = \frac{CI^2 - CW^2}{CI \times CW} \\ \times \text{Sin.} \times \text{Cos. GCM.}$$

Therefore the tang. DRC varies as Sin. $\times$ Cos. GCM, and will be a maximum when Sin. and Cos. GCM are equal, or GCM 45 degrees, or when $T=1$. According to which,

$$\text{The tang. GRD} = Y = \frac{CW}{CI} \times \frac{1}{T} = \frac{CW}{CI} = \text{tang. CIW},$$

$$\text{And tang. GRC} = X = \frac{CI^2}{CW^2} \times Y = \frac{CI}{CW} = \text{tang. CWL}$$

$$\text{But } \frac{CW}{CI} \times \frac{CI}{CW} = 1. \text{ Therefore the angles GRC, GRD,} \\ \text{are complements to each other, and IW parallel to CR, when} \\ \text{the angle DRC is greatest. And by substituting for } T, \text{ in the} \\ \text{equation tang. DRC} = \frac{CI^2 - CW^2}{CI \times CW} \times \frac{T}{1 + T^2}, \text{ we have tang.} \\ \text{DRC} = \frac{CI^2 - CW^2}{2 CI \times CW}.$$

That is, $2 CI \times CW : (CI + CW) (CI - CW) :: \text{Rad.} : \text{Tang. DRC.}$

If the ellipse be nearly a circle, then $2 CI$ or $2 CW$, would be nearly equal to $CI + CW$, in which case, $\text{tang. DRC} = \frac{CI - CW}{CI}$
 $\frac{WL}{\frac{1}{2} HI}$ very nearly when the angle DRC is a maximum.

Note to Prop. XLI.

$$\begin{aligned} \text{If } CH &= 1 \\ CW &= c \\ \angle CFR &= z \\ CF &= w \end{aligned} \quad \left\{ \begin{array}{l} \text{Then } FR = \frac{CW^2}{CH - CF \times C} = \frac{1}{1 - w \cos. z} \times \\ c^2 = (\text{by division}) c^2(1 + w \cos. z + w^2 \cos.^2 z + \\ w^3 \cos.^3 z + \&c.) \text{ By trig. } \cos.^2 z = \frac{1}{2} + \frac{1}{2} \cos. 2z, \\ \cos.^3 z = \frac{1}{4} \cos. z + \frac{1}{4} \cos. 3z, \text{ and (Prop. VI.) } c^2 = \end{array} \right.$$

$1 - w^2$, therefore by substitution we have

$$FR = c^2(1 + \frac{1}{2}w^2 + w \cos. z + \frac{1}{4}w^3 \cos. z + \frac{1}{2}w^2 \cos. 2z + \frac{1}{4}w^3 \cos. 3z)$$

$$= (1 - w^2) \left\{ 1 + \frac{1}{2}w^2 + (w + \frac{1}{4}w^3) \cos. z + \frac{1}{2}w^2 \cos. 2z + \frac{1}{4}w^3 \cos. 3z. \right\}$$

$$= 1 - \frac{1}{2}w^2 - \frac{1}{2}w^4 + (w - \frac{1}{4}w^3 - \frac{1}{4}w^5) \cos. z + (\frac{1}{2}w^2 - \frac{1}{2}w^4) \cos. 2z + (\frac{1}{4}w^3 - \frac{1}{4}w^5) \cos. 3z.$$

By omitting the terms affected with w^4 and w^5 ,

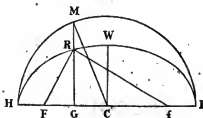
$$FR = 1 - \frac{1}{2}w^2 + (w - \frac{1}{4}w^3) \cos. z + \frac{1}{2}w^2 \cos. 2z + \frac{1}{4}w^3 \cos. 3z.$$

If the eccentricity CF be very small, then $c^2 = 1 - w^2 = 1$, nearly; and therefore all the terms connected with w^3 , w^4 , &c. may be neglected; then $FR = 1 + w \times \cos. z$, and $FR - 1 = w \times \cos. z$; hence the variation of FR is nearly in proportion to $\cos. CFR$.

PROP. XLII.

On the transverse axis HI describe a semicircle HMI , and draw the ordinate RG , which produce to M ; join MC , and draw RF , Rf to the foci.

Then $FR = CH - CF \times \cos. MCH$.



By Euclid, Book ii. Prop. 13. $FR^2 = FR^2 + fR^2 - 2FR \times fG$.

Ther. $fR^2 - FR^2 = 2FR \times fG - FR^2$.

But $fR^2 - FR^2 = (fR + FR)(fR - FR) = 2HC \times (CH - FR)2$.

And $2fF \times fG - Ff^2 = (2fG - Ff) \times Ff = (2fG - 2CF) \times 2CF = 2CG \times 2CF$.

Ther. $2HC \times (CH - FR) \times 2 = 2CG \times 2CF$; or, $CM \times (CH - FR) = CF \times CG$.

Per trig. $GC = CM \times \cos. GCM$, ther. $CH - FR = CT \times \cos. GCM$, and $FR = CH - CF \times \cos. HCM$. Ther. $Rf = CH + CF \times \cos. MCH$.

And by Prop. XLI. $Rf = \frac{CW^2}{CH} \times \frac{1}{1 - \frac{CF}{CH} \times \cos. RfH}$

Cor. 1. The $\sin. RfH : \sin. MCH :: CW : fR$.

For, Rad. : $Rf :: \sin. RfG : RG = Rf \times \sin. RfG$.

And, $CI : CW :: GM : RG = \frac{CW}{CI} \times GM$.

But, Rad. : $CM :: \sin. GCM : GM = CI \times \sin. GCM$.

Ther. $\frac{CW}{CI} \times CI \times \sin. MCH = Rf \times \sin. RfH$.

Whence $\sin. RfH : \sin. MCH :: CW : fR$.

Cor. 2. $\cos. RfH = \frac{CF + CH \times \cos. MCH}{CH + CF \times \cos. MCH}$, and

$\cos. MCH = \frac{CH \times \cos. RfH - CF}{CH - CF \times \cos. RfH}$.

For by equating the expressions for Rf . Prop. XLI. XLII.

$CH + CF \times \cos. MCH = \frac{CW^2 = CH^2 - CF^2}{CH - CF \times \cos. RfH}$; from

whence the values of $\cos. RfH$, and $\cos. MCH$, as stated in this corollary.

Cor. 3. As $\sin. \frac{RfH}{2} : \sin. \frac{MCH}{2} :: \sqrt{fT} : \sqrt{fR}$.

Put $CH = m$
 $CF = n$
 $\cos. MCH = C$
 $\cos. RfH = c$

Then $\left\{ \begin{array}{l} c = \frac{n+mC}{m+nC} \\ C = \frac{mc-n}{m-nC} \end{array} \right\}$ And per Emer. Trig. page 12.

Sin. $\frac{RfH}{2} = \sqrt{\frac{1-c}{2}} = \sqrt{\left(1 - \frac{n+mC}{m+nC}\right) \times \frac{1}{2}} = \sqrt{\frac{m+nC-n-mC}{2 \times (m+nC)}}$

$$= \sqrt{\frac{(m-n)(1-C)}{2Rf}} = \sqrt{\frac{1-C}{2}} \times \sqrt{\frac{HF}{Rf}} = \sin. \frac{MCH}{2} \times \frac{\sqrt{HF}}{\sqrt{Rf}}$$

$$\text{Hence we have, } \sin. \frac{RfH}{2} : \sin. \frac{MCH}{2} :: \frac{\sqrt{HF}}{\sqrt{Rf}} : 1 :: \sqrt{HF} : \sqrt{Rf} :: \sqrt{fI} : \sqrt{fR}$$

$$\text{Cor. 4. } fI : CW :: \text{Tang. } \frac{MCH}{2} : \text{Tang. } \frac{RfH}{2}$$

$$\text{Per trig. ib. } \text{Tang. } \frac{RfH}{2} = \sqrt{\frac{1-c}{1+c}}$$

$$1-c = 1 - \frac{n+mC}{m+nC} = \frac{m+nC-n-mC}{m+nC} = \frac{(m-n) \times (1-C)}{m+nC} = \frac{HF \times (1-C)}{Rf}$$

$$1+c = 1 + \frac{n+mC}{m+nC} = \frac{m+nC+n+mC}{m+nC} = \frac{(m+n)(1+C)}{m+nC} = \frac{IF \times (1+C)}{Rf}$$

$$\frac{1-c}{1+c} = \frac{HF \times (1-C)}{Rf} \div \frac{IF \times (1+C)}{Rf} = \frac{1-C}{1+C} \times \frac{HF}{IF} = \frac{1-C}{1+C} \times \frac{HF \times IF}{IF^2} = \frac{1-C}{1+C} \times \frac{CW^2}{fI^2}$$

$$\text{Ther. } \sqrt{\frac{1-c}{1+c}} = \text{Tang. } \frac{RfH}{2} = \text{Tang. } \frac{MCH}{2} \times \frac{CW}{fI};$$

$$\text{Ther. } 1 : \frac{CW}{fI} :: fI : CW :: \text{Tang. } \frac{MCH}{2} : \text{Tang. } \frac{RfH}{2}$$

$$\text{Cor. 5. } \sqrt{fI} : \sqrt{fH} :: \text{Tang. } \frac{MCH}{2} : \text{Tang. } \frac{RfH}{2}$$

$$\text{For (Cor. 4.) } \sqrt{\frac{1-c}{1+c}} = \sqrt{\frac{1-C}{1+C}} \times \frac{\sqrt{HF}}{\sqrt{fI}}$$

$$\text{Ther. } 1 : \frac{\sqrt{HF}}{\sqrt{fI}} :: \sqrt{fI} : \sqrt{HF} :: \sqrt{\frac{1-C}{1+C}} : \sqrt{\frac{1-c}{1+c}} ::$$

$$\text{Tang. } \frac{MCH}{2} : \text{Tang. } \frac{RfH}{2}$$

$$\text{Cor. 6. If } a=CH, a c=CF, \text{ and } c=\cos. RfI.$$

$$\text{Then, } fR : fR :: 1-c^2 : 1-2ec+c^2$$

$$\text{For by Prop. XLI. } FR = \frac{CW^2 = CH^2 - CF^2}{CH - CF \times c} = \frac{a^2 - a^2 c^2}{a - a c c} = \frac{(1 - c^2) \times a}{1 - ec},$$

$$\text{And } Rf = 2CH - FR = 2a - \frac{1 - c^2}{1 - ec} \times a = \frac{2 - 2ec - 1 + c^2}{1 - ec} \times a = \frac{1 - 2ec + c^2}{1 - ec} \times a.$$

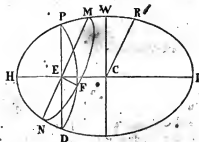
$$\text{Ther. } \frac{FR}{fR} = \frac{1 - c^2}{1 - 2ec + c^2}; \text{ or, } FR : fR :: 1 - c^2 : 1 - 2ec + c^2.$$

DEFINITION 22.

A *spheroid* is a solid conceived to be generated by the revolution of an ellipse about one of its axes, and is denominated either *prolate* or *oblate*, according to the revolution being made about the transverse or conjugate axis.

PROP. XLIII.

If a spheroid be cut by a plane in any position, except one perpendicular to the fixed axis, the section will be an ellipse.



Let NMI be the generating section, or a section of the spheroid through its axis HI, and perpendicular to the proposed section MFN; their common intersection being MN; through the intersection E, draw PED perpendicular to HI, and erect EF perpendicular to the plane NMI, and meeting the perpendicular plane in F. Then (Scholium to Prop. XIV,) we have $ME \times EN : PE \times ED :: CR^2 : CW^2$. But, by Definition 22, the points PED will be in the circumference of a circle whose

But (Prop. XXXVII.) $Pn = Cr = \frac{CH^2}{\sqrt{CH^2 + t^2} \cdot CK^2} = \frac{m^2}{a}$
 $PX = \frac{CK^2}{c\sqrt{CH^2 + t^2} \cdot CK^2} = \frac{n^2}{ca}$, and $CS = \frac{CH \times CK}{c\sqrt{CK^2 + t^2} \cdot CH^2} = \frac{mn}{cb}$.

By substituting for Cr in the value of CX , we have $CX = \frac{d}{a}$;
 and $IX \times XH = CH^2 - CX^2 = m^2 - \frac{d^2}{a^2}$.

By Scholium to Prop. XIV.

$$PX \times XZ : IX \times XH :: Pv \times vZ : qv \times vg :: CS^2 : CH^2.$$

That is, $\frac{n^2}{ca} \times XZ : m^2 - \frac{d^2}{a^2} :: (Pv)^2 : (vs)^2 :: \frac{m^2 n^2}{b^2 c^2} : m^2$,

Ther. $Pv : vs :: \frac{n}{bc} : 1 :: n : bc \therefore \frac{n^2}{ac} \times XZ = \frac{a^2 m^2 - d^2}{a^2} \times \frac{n^2}{b^2 c^2}$. Ther. $XZ = \frac{a^2 m^2 - d^2}{ac b^2}$ And $PX + XZ = PZ = 2Pv$,

that is, $\frac{n^2}{ac} + \frac{a m^2 - d^2}{ac b^2} = \frac{n^2 b^2 + a^2 m^2 - d^2}{ac b^2} = PZ = 2Pv$.

But $2Pv = \frac{2n \times vs}{bc} = \frac{n^2 b^2 + a^2 m^2 - d^2}{ac b^2} \therefore 2vs = st = \frac{n^2 b^2 + a^2 m^2 - d^2}{abn}$.

The latus-rectum (L) of the axis PZ may be thus found, $PZ : st :: st : L = \frac{n^2 b^2 + a^2 m^2 - d^2}{an^2} \times c$ (Prop. V.)

By restoring the values of a , b , and d , we have
 $n^2 b^2 + a^2 m^2 - d^2 = n^2 (n^2 + t^2 m^2) + m^2 (m^2 + t^2 n^2) - (m^2 - n^2)^2$
 $= n^4 + m^2 n^2 t^2 + m^4 + m^2 n^2 t^2 - m^4 + 2m^2 n^2 - n^4$
 $= 2m^2 n^2 t^2 + 2m^2 n^2 = (1 + t^2) \times 2m^2 n^2 = \frac{2m^2 n^2}{c^2}$.

From hence $PZ = \frac{2m^2 n^2}{ab^2 c^2}$; $st = \frac{2m^2 n^2}{abn c^2} = \frac{2m^2 n}{abc^2}$.

And $L = \frac{2m^2 n^2 \times c}{an^2 c^2} = \frac{2m^2}{ac}$; or thus,

$HB^2 - EF^2 :: CE : CT - CE :: CE : ET$; that is, $EF^2 : EP^2 :: CE : ET$.

COROLLARY 2.

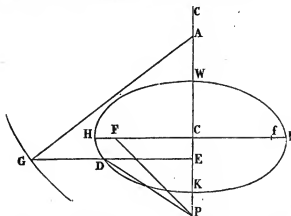
If the semicircle BAH be described on BH , the legs BA , AH of the right-angled triangle BAH , will be equal to the segments FE and EP of the right line FEP .

For $BA^2 + AH^2 = HB^2 = EF^2 + EP^2$.

Therefore $BA + AH = FE + EP = FP$.

PROP. XLVIII.

Let $HIWK$ be an ellipse, HI the greater axis, WK the lesser, C the center, F, f , the foci, P a point in WK produced, PD a line meeting the ellipse in D , and EDG perpendicular to WK : Then if EG be so taken that $FC : CK :: PD : EG$, the locus of the point G , will be in the circumference of a circle, whose center is in the axis WK , or in WK produced.



Put $CH = t$, $CK = c$, $CF = m$, $CP = d$, and $CE = x$; then $WE = c + x$, $KE = c - x$, $PE^2 = d^2 - 2dx + x^2$, and $PD^2 = \frac{m^2}{c^2} \cdot EG^2$; also, Prop. VI. $m^2 = t^2 - c^2$, and Prop. III. $ED^2 = t^2 - \frac{t^2 x^2}{c^2}$. Hence we have $PD^2 = PE^2 + ED^2 = d^2 + t^2 - 2dx + x^2 -$

$\frac{t^2 x^2}{c^2}$. But $-\frac{m^2 x^2}{c^2} = x^2 - \frac{t^2 x^2}{c^2}$, ther. $\frac{m^2}{c^2}$. $EG^2 = d^2 + t^2 - 2dx - \frac{m^2}{c^2}x^2$; an equation of a circle, whose circumference is the locus of the point G, and whose center is in the line P W.

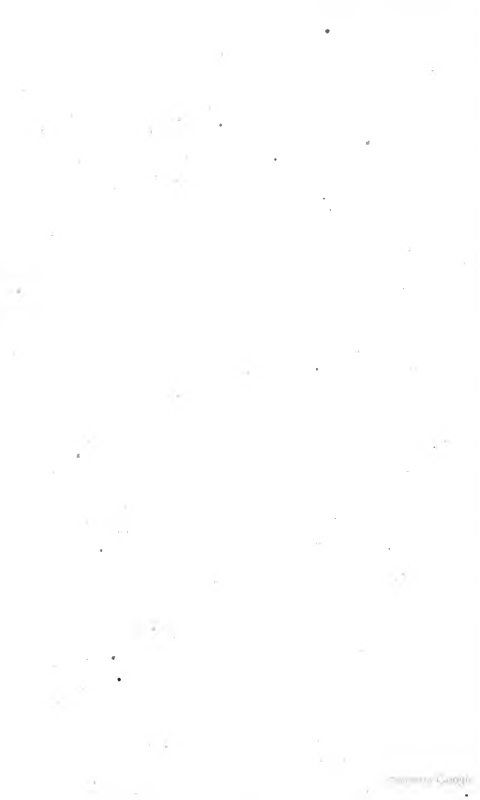
COR. 1. If the point D be taken above the transverse axis H I, ther. $PE = d + x$ and $\frac{m^2}{c^2}EG^2 = d^2 + t^2 + 2dx - \frac{m^2}{c^2}x^2$, an equation of a circle.

COR. 2. If P falls on K or W, then $CP = CK$, or $b = d$, and $m^2EG^2 = c^4 + c^2t^2 \mp 2c^2x - m^2x^2$.

COR. 3. When P coincides with C, then $PC = d = 0$, ther. $EG^2 = \frac{c^2 t^2}{m^2} - x^2$, an equation of a circle whose center is C, and radius $\frac{ct}{m}$.

COR. 4. When $FC = CK$; then $EG = PD$.

* Put $CE = x$, $EG = y$, and let $a \pm 2bx - cx^2 = cy^2$, a, b, c , being constant quantities; make $AC = \frac{b}{c}$, and $AE = z$. We then have $AE \pm AC = CE = x \pm \frac{b}{c}$ from whence $2bx = 2bz \pm \frac{2b^2}{c}$, and $cx^2 = cz^2 \pm 2bz + \frac{b^2}{c}$, then by substitution, $\frac{ac + b^2}{c^2} - z^2 = y^2$, or $r^2 - AE^2 = EG^2$; an equation of a circle whose center is A, and semi-diameter $r = \frac{1}{c}\sqrt{ac + b^2}$.



OF THE

CIRCLE OF CURVATURE.

DEFINITION.

WE know that a circle may be described through any three points taken in a given curve; and since an indefinite number of such points may be so taken, an indefinite number of circles may be described through those points; but the nearer those three points are together, the nearer will be the coincidence of the curve and circle. Therefore, as the *tangent* of a curve is the limit of all the straight lines which meet the curve in two points, so will the *osculating circle* be the limit of all the circles which pass through any three points in the given curve.

Hence we may conclude, that a circle of equal curvature with a curve at any given point therein, is that which passes through three points of the curve, which are supposed *indefinitely* near to each other; and therefore have the same common ordinate, chord, arch, and tangent, at the point of contact.

The following extract from Mr. Whiston's Euclid, page 68, is worthy of remark:—

1. Circles growing into amplitude greater than any given one, approach always, even unto infinity, nearer and nearer to the tangent, but are never joined to it, otherwise than in one single point of contact; which thing, although it be most evident, is yet truly admirable.

focus; and let $PQVL$ be the circle of curvature touching it in P , whose diameter is PL , and PV the chord of curvature passing through the center C . The other lines drawn as per figure.

From the similar triangles PNQ , PVQ , we have $PN : PQ :: PQ : PV = \frac{PQ^2}{PN} = \frac{\text{arc}^2 PQ}{PN} \therefore PQ^2 = PN \times PV$. And (Prop. XVI. ellip.) $PN \times NG : NQ^2 :: PC^2 : CD^2 \therefore NQ^2 = \frac{PN \times NG \times CD^2}{PC^2}$. But per lemma 2, $PQ^2 = NQ^2 \therefore PN \times PV = \frac{PN \times NG \times CD^2}{PC^2}$, ther. $PV = \frac{NG \times CD^2}{PC^2} = \frac{2PC \times CD^2}{PC^2} = \frac{2CD^2}{PC}$. For when Q moves up to P , NG is equal to $2PC$.

COR. 1. The chord of curvature PV , passing through the center C , is equal to the parameter of the diameter PG . (Ellip. Def. 18.)

COR. 2. From the similar triangles PaQ , PdQ , we have $Pa : PQ :: PQ : Pd \therefore Pa = \frac{PQ^2}{Pd}$. Therefore $PN \times PV = Pa \times Pd$.

PROP. II.

To determine the diameter of the circle of curvature at any point of an ellipse.

By the similar triangles PCA , PVL (Fig. to Prop. I.) $PA : PC :: PV : PL = \frac{PV \times PC}{PA}$, but $PV = \frac{2DC^2}{PC}$ (last Prop.)

Ther. $PL = \frac{PC}{PA} \times \frac{2DC^2}{PC} = \frac{2DC^2}{PA} = \text{diameter of curvature}$.

PROP. III.

To determine the chord of the circle of curvature at any point of an ellipse that passes through the focus thereof.

Join PF , and let it intersect the circle of curvature in a , and the conjugate diameter DB in E ; also join aL . (Fig. to Prop. I.) Then per the similar triangles PAE , PaL ; $PE : PA :: PL :$

$Pa = \frac{PA \times PL}{PE}$, but (Cor. Prop. XXV. ellip.) $PE = CH$, and
 (Prop. II.) $PL = \frac{2DC^2}{PA}$; ther. $Pa = \frac{PA}{CH} \times \frac{2DC^2}{PA} = \frac{2DC^2}{CH}$
 = chord of curvature passing through the focus F.

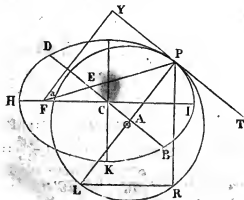
Cor. 1. By Prop. I. $PV = \frac{2CD^2}{PC}$, and by this Prop. $Pa = \frac{2DC^2}{CH}$. Hence $PV : Pa :: \frac{1}{PC} : \frac{1}{CH} :: CH : CP$.

Cor. 2. At the extremity K of the minor axis, CD becomes CH, ther. $Pa = \frac{2CD^2}{CD} = 2DC$.

Cor. 3. Since by Prop. I. $PV = \frac{2CD^2}{PC}$, by Prop. II. $PL = \frac{2DC^2}{PA}$, and by Prop. III. $Pa = \frac{2DC^2}{CH}$ we have the diameter of curvature, the chord of curvature passing through the centre, and the chord of curvature passing through the focus respectively, as $\frac{1}{PA}, \frac{1}{PC}, \frac{1}{PE}$.

PROP. IV.

If FY be drawn perpendicular to the tangent at P, and L represent the latus-rectum of the transverse axis, then the diameter of curvature $PL = L \times \text{Sec.}^2 PFY$.



PROP. VI.

The radius of curvature $P\odot$ at any point P of an ellipse, is directly as the cube of the semi-diameter CD .

By Cor. 1. Prop. XXXI. Ellip. $PA = \frac{CH \times CK}{CD}$ (Fig. to Prop. IV.)

And (Prop. II.) $P\odot = \frac{DC^3}{PA}$; and by substituting for PA we have $P\odot = DC^3 \times \frac{CD}{CH \times CK} = \frac{CD^3}{CH \times CK}$. But CH and CK are given, therefore the radius of curvature $P\odot$ is directly as CD^3 .

COR. 1. The radius of curvature at the vertex of the transverse diameter is half the latus-rectum of that diameter.

For when P coincides with I , CD becomes equal to CK , and then $P\odot = \frac{CD^3}{CH \times CK} = \frac{CK^3}{CH \times CK} = \frac{CK^2}{CH}$ = half the latus-rectum of the transverse axis (Def. 18. Ellip.).

COR. 2. If the point P falls on K , CD will become equal to CH , and then $P\odot = \frac{CD^3}{CH \times CK} = \frac{CH^3}{CH \times CK} = \frac{CH^2}{CK}$ = half the latus-rectum of the conjugate axis (Def. 18. Ellip.).

COR. 3. The radius of curvature is therefore *least* at I , and *greatest* at K .

COR. 4. Since the radius of curvature at H , is to the radius of curvature at K , as $CK^3 : CH^3$,

By putting d for the measure of a degree at H ,

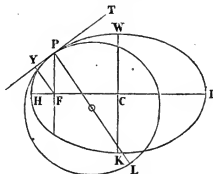
And - - - D for the measure of a degree at K , we shall have $d : D :: CK^3 : CH^3$ (the lengths of the degrees being as the radii). Hence if d be less than D , CK will be less than CH , which is found to be the case by actual measurements taken at the Equator and near the North Pole of the Earth.

COR. 5. Any chord of curvature PR , is directly as the sine of the angle RPT , and as the cube of the semi-diameter CD .

For $\text{rad.} : PL :: \sin. PLR : PR$; that is, $1 : \frac{2CD^3}{CH \times CK} :: \sin. RPT : PR = \frac{2}{CH \times CK} \times CD^3 \times \sin. RPT$.

PROP. VII.

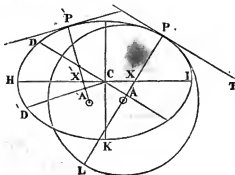
If PT be a focal tangent to the ellipse $HWIK$, the radius of curvature at the point P is equal to $\frac{FP^3}{FY^2}$.



By Prop. IV. $PL = \frac{FP^3}{FY^2} \times L$, and Def. 6. and Prop. XV, Ellip. $2FP = L$. Ther. $PL = \frac{FP^3}{FY^2} \times 2FP$; or, $\frac{PL}{2} = P\odot = \frac{FP^3}{FY^2}$.

PROP. VIII.

If PA , PX , be perpendicular to the tangent PT of an ellipse, then the radius of curvature $P\odot$ is *reciprocally* as the cube of PA , or *directly* as the cube of PX .



By Cor. 1. Prop. XXXI. Ellip. $CD^3 = \frac{CH^3 \times CK^3}{PA^3}$, and Prop. VI. $P\odot = \frac{CD^3}{CH \times CK}$, and substituting for CD^3 , we have $P\odot = \frac{1}{CH \times CK} \times \frac{CH^3 \times CK^3}{PA^3} = \frac{CH^2 \times CK^2}{PA^3}$, but CH and CK are constant, therefore $P\odot$ is as $\frac{1}{PA^3}$, or $P\odot$ is reciprocally as PA^3 .

And since $P\odot \times PA^3 = CH^2 \times CK^2$, and (Prop. XXVII. Ellip.) $PA \times PX = CK^2$; ther. $PA^2 = \frac{CK^2}{PX}$; and by substitution $P\odot \times \frac{CK^2}{PX} = CH^2 \times CK^2$; or, $P\odot = \frac{CH^2}{CK^2} \times PX$; therefore $P\odot$ is directly as PX .

Cor. 1. By Prop. XXXVII. Ellip. $PX = \frac{CK^2}{c\sqrt{CH^2 + t^2 \cdot CK^2}}$.

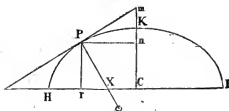
Ther. $\frac{CH^2}{CK^2} \times PX^2 = \frac{CK^2}{(c\sqrt{CH^2 + t^2 \cdot CK^2})^2} \times \frac{CH^2}{CK^2}$.

That is, $P\odot = \frac{CK^2 \times CH^2}{(c\sqrt{CH^2 + t^2 \cdot CK^2})^2}$; $c = \cos$; $t = \tan$. PXL

Cor. 2. If $P\odot$, the radius of curvature at any other point $\dot{P}$, intersect the transverse axis in $\dot{X}$, and the semidiameter CD in $\dot{A}$; and if d represent the measure of a degree at P , and D the measure of a degree at $\dot{P}$, then by the Prop. $P\odot : \dot{P}\odot :: d : D :: \frac{1}{PA^3} : \frac{1}{\dot{P}\dot{A}^3} :: PX^2 : \dot{P}\dot{X}^2$. Or $\frac{D}{d} = \frac{PA^2}{\dot{P}\dot{A}^2} = \frac{\dot{P}\dot{X}^2}{PX^2}$.

PROP. IX.

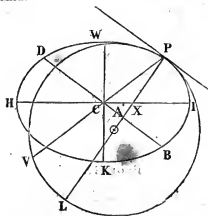
If the radius of curvature $P\odot$, perpendicular to the tangent Pm , intersect the transverse diameter HI in X , and the ordinates Pn, Pr be drawn, then $\frac{\text{Sec.}^2 n P m}{P\odot} = \frac{CK^4}{CH^2 \times Cn^2}$.



By Prop. VIII. $P\odot = \frac{CH^2}{CK^4} \times PX^2$. and by trig. rad. : sec.
 $rPX :: Pr : PX$; ther. $PX = Pr \times \sec. rPX$, and by substitution we have $P\odot = \frac{CH^2}{CK^4} \times Pr^2 \times \sec.^2 rPX \therefore \frac{\sec.^2 n Pm}{P\odot} = \frac{CK^4}{CH^2 \times Cn^2}$.

PROP. X.

If $P\odot$ be the radius of curvature at any point P, BD conjugate to PC, HI and WK the transverse and conjugate axes, and PA perpendicular to BC, then $P\odot$, CB, PA are in continued proportion.



By Prop. LI. $P\odot = \frac{CD^2}{CH \times CK}$, and Cor. 1. Prop. XXXI.

Ellip, $PA \times CD = CH \times CK$. Then substituting for $CH \times CK$, we have $P\odot = \frac{CD^2}{PA \times CD} = \frac{CD^2}{PA}$; hence $P\odot$, CD , PA , are in continued proportion.

PROP. XI.

$PA^3 : CB^3 :: \frac{1}{2}$ parameter of the transverse axis HI : rad. curvature $P\odot$. $PA^3 : CK^3 :: \frac{1}{2}$ parameter of the conjugate axis KW : radius of curvature $P\odot$.

By Prop. VIII. $P\odot \times PA^3 = CH^2 \times CK^2 = HC^2 \times \frac{CK^2}{HC}$.

Ther. $PA^3 : CB^3 :: \frac{CK^2}{HC} : P\odot :: \frac{1}{2}$ param. of HI : $P\odot$.

From the same equation $P\odot \times PA^3 = CH^2 \times CK^2 = CK^2 \times \frac{HC^2}{CK}$, we have $PA^3 : CK^3 :: \frac{HC^2}{CK} : P\odot :: \frac{1}{2}$ param. of KW : $P\odot$ (fig. to last Prop.).

PROP. XII.

The chord which the circle of curvature cuts off from a diameter of an ellipse, is a third proportional to that diameter and its conjugate; which chord will be the parameter of the diameter.

By Prop. I. The chord of curvature PV passing through the center C of the ellipse is equal to $\frac{2CD^2}{PC}$; ther. $2PC : 2CD :: 2CD : \frac{2CD^2}{PC} = PV$.

PROP. XIII.

If PX be perpendicular to the tangent at P , intersecting the transverse axis HI in X , and L represent the parameter of the transverse diameter.

Then $\frac{PX^2}{P\odot} = \left(\frac{L}{2}\right)^2$.

By Prop. VIII. $P\odot = \left(\frac{CH}{CK}\right)^2 \times PX^2$; but (Def. 18.) $\frac{CK^2}{CH}$

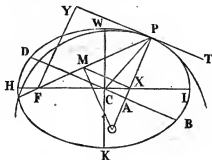
$$= \frac{L}{2} \quad \text{Ther. } \frac{CH}{CK^2} = \frac{2}{L}; \text{ hence } P\odot = \frac{4 \times PX^2}{L^2} = \left(\frac{2}{L}\right)^2 \times PX^2.$$

$$\text{Ther. } \frac{PX^2}{P\odot} = \left(\frac{L}{2}\right)^2. \quad (\text{Fig. to last Prop.})$$

PROP. XIV.

Let a perpendicular be drawn to the tangent at P, intersecting the transverse axis HI in X, and PF drawn to the focus F.

Then if XM be drawn perpendicular to PX, and M $\odot$ perpendicular to PF, intersecting PX in $\odot$; then will the point $\odot$ be the center of the circle of curvature at the point P.



Draw DB conjugate to PC, and demit the perpendicular FY on the tangent PT.

By Prop. XXVII. Ellip. $PA \times PX = CK^2$

By Prop. II. $PA \times P\odot = CD^2$.

Ther. $CD^2 : CK^2 :: P\odot : PX$.

By Prop. XXXI. Ellip. $FP^2 : FY^2 :: CD^2 : CK^2$, and per. sim. triangles $FP^2 : FY^2 :: P\odot^2 : PM^2 :: P\odot : PX :: P\odot^2 : PX \times P\odot$; that is, $P\odot^2 : PM^2 :: P\odot^2 : PX \times P\odot \therefore P\odot \times PX = PM^2$.

Consequently MX is at right angles to the radius of curvature $\odot P$.

$$\frac{a^2 b^2}{(a^2 - v^2 S^2)^{\frac{3}{2}}}, \text{ or, by substituting } 1 - C^2 \text{ for } S^2; R = \frac{a^2 b^2}{(b^2 + v^2 C^2)^{\frac{3}{2}}}.$$

$$\text{When } P \text{ coincides with } I, \text{ then } S = 0, \text{ and } R = \frac{a^2 b^2}{(a^2)^{\frac{3}{2}}} = \frac{a^2 b^2}{a^3}.$$

$$= \frac{b^2}{a} = \text{half the latus-rectum of the transverse axis.}$$

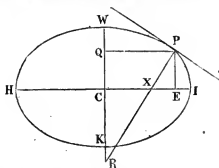
$$\text{When } P \text{ coincides with } W, \text{ then } C = 0, \text{ and } R = \frac{a^2 b^2}{(b^2)^{\frac{3}{2}}} = \frac{a^2 b^2}{b^3}.$$

$$= \frac{a^2}{b} = \text{half the latus-rectum of the conjugate axis.}$$

See Corollaries 1 and 2. Prop. VI.

PROP. XVI.

Having the meridional degree, and also the degree perpendicular to the meridian, in a given latitude; to find the earth's axes, supposing it an ellipsoid.—(Trigonometrical Survey, vol. i. page 300, and Mathematical Repository, No. 14.)



Suppose IKHW to be the elliptical meridian passing through the point P, whose latitude is given; CI, CW, the equatorial and polar semi-axes. Let PE be the ordinate to the point P,

* Otherwise thus:

Join CP, and draw its semi-conjugate Cp, and we have (Prop. VI.)
rad. cur. at H : rad. cur. at P :: CK² : Cp²; but (Cor. 1. *ibid.*) The rad.

and draw PR perpendicular to the curve at P , which will be the radius of curvature of the perpendicular degree at that point; also draw PQ parallel to IC .

Put s , c , t for the sine, cosine, and tangent of the given latitude PXE .

P = length of the perpendicular degree.

m = length of the meridional degree.

$d = 57^{\circ}. 29$, &c.

$$\text{Then } CE = QP = \frac{CI^2}{\sqrt{CI^2 + t^2 CW^2}} \text{ --- (Prop. XXXVII. Ellip.)}$$

$$PR = \frac{CI^2}{c\sqrt{CI^2 + t^2 CW^2}} = dP \text{ (Prop. XLIV. Ellip.)}$$

$$\text{And } \text{---} \frac{CI^2 \cdot CW^2}{(c\sqrt{CI^2 + t^2 CW^2})^3} = dm \text{ (Cor. 1. Prop. VIII.)}$$

$$\text{Therefore } 1 : \frac{CW^2}{c^2 CI^2 + c^2 t^2 CW^2} :: P : m \therefore \frac{CI^2}{CW^2} = \frac{P}{mc^2} - t^2.$$

$$\text{But } c^2 = \frac{1}{1+t^2} \therefore \frac{CI^2}{CW^2} = \frac{P(1+t^2)}{m} - t^2 = \frac{P + (P-m)t^2}{m}, \text{ which}$$

put = V .

Hence $CI^2 = v \times CW^2$; substitute for CI^2 in the value of dP ,

$$\text{Then } \frac{v CW^2}{c\sqrt{v CW^2 + t^2 CW^2}} = dP = \frac{v \cdot CW}{c\sqrt{v + t^2}} \therefore CW = \frac{cdP}{v\sqrt{v + t^2}}.$$

$$\text{cur. at } H = \frac{CK^2}{CH} = \frac{b^2}{a}; \text{ hence } \frac{b^2}{a} : b^2 :: \text{rad. cur. at } P : Cp^1 \text{ rad.}$$

$$\text{cur. at } P = \frac{Cp^1}{ab}. \text{ But (Prop. XXXVII. Ellip.) } Cp = \frac{ab}{c\sqrt{b^2 + a^2 t^2}} =$$

$$\frac{ab}{\sqrt{(a^2 - b^2)s^2 + b^2}} = \frac{ab}{\sqrt{b^2 + v^2 s^2}}, \text{ ther. } Cp^1 = \frac{a^2 b^1}{(b^2 + v^2 s^2)^{\frac{1}{2}}} \text{ (} s = \sin, c =$$

cos., $t = \tan$, of pCH , or of PtH , or of the comp. of PXt , ther. $s = C$).

The rad. cur. at P being equal to $\frac{1}{ab} \times Cp^1$, we have $R = \frac{1}{ab} \times$

$$\frac{a^2 b^1}{(b^2 + v^2 C^2)^{\frac{1}{2}}} = \frac{a^2 b^2}{(b^2 + v^2 C^2)^{\frac{1}{2}}} \text{ as before.}$$

$$\text{We have } v = \frac{P + (P-m)t^2}{m} = \frac{P + (P-m)\frac{s^2}{c^2}}{m} = \frac{P + \frac{Ps^2 - ms^2}{c^2}}{m}$$

$$= \frac{Pc^2 + Ps^2 - ms^2}{mc^2} = \frac{P - ms^2}{mc^2}.$$

$$\text{And } v + t^2 = \frac{P - ms^2}{mc^2} + \frac{s^2}{c^2} = \frac{Pc^2 - ms^2c^2 + ms^2c^2}{mc^4} = \frac{Pc^2}{mc^4}$$

$$= \frac{P}{mc^2}.$$

$$\text{Ther. } CW = \frac{cdP}{v} \sqrt{v + t^2} = cdP \times \frac{mc^2}{P - ms^2} \times \frac{1}{c} \sqrt{\frac{P}{m}} =$$

$$\frac{c^2 d P m \sqrt{P}}{P - ms^2} = \frac{c^2 d P \sqrt{P m}}{P - ms^2} = \frac{c^2 d \sqrt{P m}}{1 - \frac{m}{P} s^2} = \frac{c^2 d \sqrt{P m}}{(1 + s\sqrt{\frac{m}{P}})(1 - s\sqrt{\frac{m}{P}})}$$

$$CI^2 = v \times CW^2 = v \times \frac{c^2 d^2 P^2}{v^2} \times (v + t^2) = \frac{c^2 d^2 P^2}{v} \times (v + t^2) =$$

$$c^2 d^2 P^2 \times \frac{mc^2}{P - ms^2} \times \frac{P}{mc^2} = \frac{c^2 d^2 P^2}{P - ms^2} = \frac{c^2 d^2 P^2}{1 - \frac{m}{P} s^2}.$$

$$\text{Ther. } CI = \frac{cdP}{\sqrt{1 - \frac{m}{P} s^2}} = \frac{cdP}{\left\{ (1 + s\sqrt{\frac{m}{P}})(1 - s\sqrt{\frac{m}{P}}) \right\}^{\frac{1}{2}}}.$$

COROLLARY I.

If l = the length of a *degree of longitude* at the point P , then PQ will be its radius of curvature and equal to dl , and $PR = dP$; therefore $PQ : PR :: l : P$; $c : l \therefore P = \frac{l}{c}$, which being substituted in the above expressions, we have

$$CW = \frac{c^2 d \sqrt{P m}}{1 - \frac{m}{P} s^2} = \frac{dc \sqrt{cm l}}{1 - \frac{mc}{l} s^2} = \frac{dc \sqrt{cm l}}{(1 + s\sqrt{\frac{mc}{l}})(1 - s\sqrt{\frac{mc}{l}})}, \text{ and}$$

$$CI = \frac{cdP}{\sqrt{1 - \frac{m}{P} s^2}} = \frac{dl}{\left\{ (1 + s\sqrt{\frac{mc}{l}})(1 - s\sqrt{\frac{mc}{l}}) \right\}^{\frac{1}{2}}}$$

COROLLARY 2.

Because $\frac{CI^2}{c\sqrt{CI^2+t^2CW^2}} = PR = dP$; if b and T represent the *cosine* and *tangent* of some other latitude, and P the *perpendicular degree* in that latitude; then $\frac{CI^2}{b\sqrt{CI^2+T^2CW^2}} = dP$, the radius of curvature where the perpendicular P is measured. Hence $\frac{CI^2}{Pb\sqrt{CI^2+T^2CW^2}} = d$, and the former equation gives $\frac{CI^2}{Pc\sqrt{CI^2+t^2CW^2}} = d$; these being equated, we have $P^2b^2(CI^2+T^2CW^2) = P^2c^2(CI^2+t^2CW^2)$.

Let s and S be the *sines* to the *cosines* c and b ; put $\frac{s^2}{c^2}$ and $\frac{S^2}{b^2}$ for t^2 and T^2 , and we shall have $P^2b^2(CI^2 + \frac{S^2}{b^2} \cdot CW^2) = P^2c^2(CI^2 + \frac{s^2}{c^2} \cdot CW^2)$.

And by multiplying and transposing, we get $(P^2b^2 - p^2c^2) \times CI^2 = (p^2s^2 - P^2S^2) \times CW^2$; hence we have $CI : CW :: \sqrt{p^2s^2 \propto P^2S^2} : \sqrt{P^2b^2 \propto p^2c^2}$, for the ratio of the axes; which being expounded by $1 : n$, we have $CI^2 : CW^2 :: n^2 : 1$. $\therefore CI^2 = n^2 \times CW^2$; this substituted for CI^2 in the equation

$$\frac{CI^2}{Pc\sqrt{CI^2+t^2CW^2}} = d, \text{ gives } \frac{n^2 \cdot CW^2}{Pc\sqrt{n^2 \cdot CW^2+t^2 \cdot CW^2}} = \frac{n^2 \cdot CW}{Pc\sqrt{n^2+t^2}} = d \therefore CW = \frac{dcP}{n^2} \sqrt{n^2+t^2}. \text{ Whence } CI = n \times CW = \frac{dcP}{n} \sqrt{n^2+t^2}. \quad n = \sqrt{\frac{p^2s^2 \propto P^2S^2}{P^2b^2 \propto p^2c^2}}.$$

Hence if l and L be the *degrees of longitude* in the given latitudes, we have $p = \frac{l}{c}$, and $P = \frac{L}{b}$, which substituted for p and P in the proportion $CI : CW :: \sqrt{p^2s^2 \propto P^2S^2} : \sqrt{P^2b^2 \propto p^2c^2}$, we shall have $CI^2 : CW^2 :: l^2t^2 \propto L^2T^2 : L^2 \propto l^2 :: \pi^2 : 1$.

Ther. $\pi = \sqrt{\frac{l^2 t^2 \omega L^2 T^2}{L^2 \omega l^2}}$; hence $CW = \frac{dl}{\pi^2} \sqrt{\pi^2 + t^2}$, and $CI = \frac{dl}{\pi} \sqrt{\pi^2 + t^2}$.

If $CI^2 = n^2 \times CW^2$; or $CI^2 = \pi^2 \times CW^2$ be substituted in the equation $\frac{CI^2}{Pb\sqrt{CI^2 + T^2} \cdot CW^2} = d$, we shall obtain

$$CW = \frac{dbP}{n^2} \sqrt{n^2 + T^2}, \text{ and } CI = \frac{dbP}{n} \sqrt{n^2 + T^2}.$$

Or,

$$CW = \frac{dl}{\pi^2} \sqrt{\pi^2 + T^2}, \text{ and } CI = \frac{dl}{n} \sqrt{\pi^2 + T^2}.$$

The values of n and π remaining the same.

COROLLARY 3.

If H = an arc, corresponding to the nat. sin. $s\sqrt{\frac{m}{p}}$ (rad. 1.) then by trigonometry, $(1 + s\sqrt{\frac{m}{p}})(1 - s\sqrt{\frac{m}{p}}) = \sin.(90^\circ + H)$
 $\sin.(90^\circ - H) = \cos.^2 H$. And by substitution $CW = d\sqrt{pm}$
 $\times \frac{\cos.^2 \text{lat.}}{\cos.^2 H}$, $CI = dp \times \frac{\cos. \text{lat.}}{\cos. H}$, and $\frac{CW}{CI} = \sqrt{\frac{m}{p}} \times \frac{\cos. \text{lat.}}{\cos. H}$.

If $s\sqrt{\frac{m}{p}}$ be considered as a cosine, then the *sine* of H must be used.

COROLLARY 4.

If G = an arc, corresponding to the nat. sin. $s\sqrt{\frac{mc}{l}}$, then $(1 + s\sqrt{\frac{mc}{l}})(1 - s\sqrt{\frac{mc}{l}}) = \sin.(90^\circ + G) \sin.(90^\circ - G) = \cos.^2 G$. And by substitution $\frac{dc\sqrt{cm}l}{\cos.^2 G} = CW$, $\frac{dl}{\cos. G} = CI$, and $\frac{CW}{CI} = \frac{l \times \cos. G}{c\sqrt{cm}l}$.

If $s\sqrt{\frac{mc}{l}}$ be considered as a cosine, then the *sine* of G must be used.

p = length of the perpendicular degree,

$dp = RG = RA$ = radius of curvature corresponding to p ,

s = sine, and c = cos. of the angle FRO .

Then in the elliptic quadrant FRG (FRA) are given the semi-transverse axis $RG = dp$, and the radius of curvature at G , in direction EGP , or $FGS = dm$, to find the semi-conjugate axis RF .

$$(\text{Cor. I. Prop. VI.}) \frac{FR^2}{RG} = dm \therefore FR^2 = Rg \times dm = pmd^2.$$

In the elliptic quadrant FRA are given $FR^2 = pmd^2$; $RA = dp$; and s and c , the sine and cos. of the angle FRO , to find RO^2 .

$$(\text{Prop. XXXVII. Ellip.}) RO^2 = \frac{RF^2 \times RA^2}{s^2 RF^2 + c^2 RA^2} = \frac{pmd^2 s^2}{pmd^2 s^2 + p^2 d^2 c^2} = \frac{mp^2 d^2}{ms^2 + pc^2}.$$

In the elliptic quadrant GRO (right angled at R), are given $GR = dp$, and $RO^2 = \frac{mp^2 d^2}{ms^2 + pc^2}$; to find R the radius of curvature at the vertex G , in Direction GO . (Cor. Prop. VI.) $R = \frac{RO^2}{RG} = \frac{mp^2 d^2}{ms^2 + pc^2} \div dp = \frac{mpd}{ms^2 + pc^2}$, therefore $\frac{R}{d} = \frac{mp}{ms^2 + pc^2} = \frac{mp}{ms^2 - ps^2 + p} = \frac{mp}{p - (p-m)s^2}$ = length of a degree oblique to the meridian. ($1 - s^2 = c^2$).

Cor. I. If Δ and D represent the lengths of two oblique degrees; s , c , and S , C , the respective sines and cosines of their inclination to the meridian; then $\Delta = \frac{pm}{ms^2 + pc^2}$, and $D = \frac{pm}{mS^2 + pC^2}$; from whence $p = \frac{\Delta ms^2}{m - \Delta c^2} = \frac{Ds^2 m}{m - C^2 D}$, and $m = \frac{\Delta c^2 p}{p - s^2 \Delta} = \frac{C^2 D p}{p - S^2 D}$; therefore $m = \frac{S^2 c^2 - C^2 s^2}{S^2 D - s^2 \Delta} \times \Delta D$, and $p = \frac{S^2 c^2 - C^2 s^2}{c^2 \Delta - C^2 D} \times \Delta D$, the meridional and perpendicular degrees, exhibited in terms of the oblique degrees, combined with

the sines and cosines of their inclinations to the meridian. Therefore an ellipsoid may be determined from the lengths of two oblique degrees in the same latitude.

We may remark, that $\frac{p m}{p - (p - m)s^2}$ will give the oblique degree on different spheroids, because the expression is in terms of the meridional and perpendicular degrees and the sine of the obliquity only.

When R O coincides with R A, then $s=1$ and $c=0$; in that case $\Delta = \frac{p m}{m s^2 + p c^2} = \frac{p m}{m} = p$.

Cor. 2. Since $\Delta = \frac{p m}{p - (p - m)s^2} = \frac{m}{1 - \frac{p}{p - m} s^2} = \frac{m}{1 - v^2 s^2} = \frac{m}{(1 + v s)(1 - v s)}$ by putting $\frac{p}{p - m} s^2 = v^2$. If A = an arc corresponding to the nat. sin. $v s$ (radius unity), then per trig. $(1 + v s)(1 - v s) = \sin. (90^\circ + A) \sin. (90^\circ - A) = \cos.^2 A$; therefore $\Delta = \frac{m}{\cos.^2 A}$. Hence the following rule.

Find the log. $s\sqrt{\frac{p - m}{p}}$ among the log. sines;

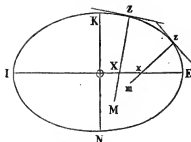
Double the log. cosine corresponding thereto,

Subtracted from the logarithm of m , and

The remainder will be the logarithm of the oblique degree.

PROP. XVIII.

To find the earth's axes, having given the measures of a degree of a meridian in two given latitudes, the earth being supposed an ellipsoid.—(*Mathematical Repository*, No. 15, November, 1815.)



Let I K E N represent a meridian of the earth, K N the less, and I E the greater axis, and z, z, the given latitudes; at right angles to which let Z X, z x be drawn, and let Z M, z m represent the radii of curvature at Z and z.

Put A = degrees in the greater latitude; S = sine, C = cosine;
 B = degrees in the less latitude; s = sine, c = cosine; rad. 1.
 D = length of a degree on the meridian, in latitude A,
 d = length of a degree on the meridian, in latitude B,

E = an arc, corresponding to the nat. sin. $s \sqrt{\frac{d}{D}} = v s$,

F = an arc, corresponding to the nat. cosine $c \sqrt{\frac{d}{D}} = v c$,

57.29, &c. $\times D = R = Z M$; 57.29, &c. $\times d = r = z m$,

57.29, &c. being the degrees in a circular arc equal to rad.

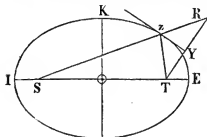
Put also $O E^2 = a^2$, $O K^2 = b^2$, and L = principal latus-rectum.

Then Prop. XV. $\left(\frac{a^2 - (a^2 - b^2) S^2}{a^2 - (a^2 - b^2) s^2} \right)^{\frac{1}{2}} = \frac{d}{D} \therefore (1 - v^2) a^2 = (S^2 - v^2 s^2) (a^2 - b^2)$, and thence $b^2 : a^2 :: v^2 c^2 - C^2 : S^2 - v^2 s^2$;
 Or, $\frac{O K^2}{O E^2} = \frac{(v c + C)(v c - C)}{(S + v s)(S - v s)}$. Hence the ratio of O K to O E is known.

The proportion of the diameters being known, the principal latus-rectum may be found as follows.

* $\frac{O K^2}{O E^2} = \frac{(v c + C)(v c - C)}{(S + v s)(S - v s)} = \frac{(c d^{\frac{1}{2}} + C D^{\frac{1}{2}})(c d^{\frac{1}{2}} - C D^{\frac{1}{2}})}{(S D^{\frac{1}{2}} + s d^{\frac{1}{2}})(S D^{\frac{1}{2}} - s d^{\frac{1}{2}})}$, by substituting for v. The same as given in vol. iii. page 144, Doct. Hutton's Course.

From the foci S, T , draw Sz, Tz ; also draw TR at right angles to the tangent zy , meeting Sz produced in R .



Then (6. Ellip.) $\frac{ST}{2} = \sqrt{(a^2 - b^2)}$, and (Prop. IV.) $\frac{L}{2} = \frac{OK^2}{OE}$
 $= \cos.^2 Y T z \times r$. And per trig. $a : \sqrt{(a^2 - b^2)} :: \sqrt{(S^2 - v^2 s^2)} :$
 $\sqrt{(1 - v^2)} :: s : \sin. Y T z = s \sqrt{\frac{1 - v^2}{S^2 - v^2 s^2}}$, hence the $\cos. Y T z$
 $= \sqrt{\frac{S^2 - s^2}{S^2 - v^2 s^2}}$; therefore $\frac{OK^2}{OE} = \left(\frac{(S+s)(S-s)}{(S+vs)(S-vs)} \right)^{\frac{1}{2}} \times r$.

By using the sine (S) of the greater latitude, we have $\frac{OK^2}{OE} =$
 $\left(\frac{(S+s)(S-s)}{(S+vs)(S-vs)} \right)^{\frac{1}{2}} \times v^2 \times R$.

Hence by having the values of $\frac{OK^2}{OE^2}$ and $\frac{OK^2}{OE}$ as above, we readily obtain

$$OK = \left(\frac{(S+s)(S-s)}{(vc+C)(vc-C)} \right)^{\frac{1}{2}} \times \frac{(S+s)(S-s)}{(S+vs)(S-vs)} \times r,$$

$$OE = \left(\frac{(S+s)(S-s)}{(S+vs)(S-vs)} \right)^{\frac{1}{2}} \times \frac{(S+s)(S-s)}{(vc+C)(vc-C)} \times r.$$

But by Trigonometry,

$$(S+s)(S-s) = \sin. (A+B) \sin. (A-B),$$

$$(S+vs)(S-vs) = \sin. (A+E) \sin. (A-E),$$

$(vc+C)(vc-C) = \sin. (A+F) \sin. (A-F)$. Therefore by substitution,

$$\frac{OK^2}{OE^2} = \frac{(vc+C)(vc-C)}{(S+vs)(S-vs)} = \frac{\sin.(A+F) \sin.(A-F)}{\sin.(A+E) \sin.(A-E)},$$

$$\frac{OK^2}{OE^2} = \left(\frac{(S+s)(S-s)}{(S+vs)(S-vs)} \right)^{\frac{1}{2}} \times r = \left(\frac{\sin.(A+B) \sin.(A-B)}{\sin.(A+E) \sin.(A-E)} \right)^{\frac{1}{2}} \\ \times 57.29 \text{ \&c.} \times d. \text{ And thence}$$

$$OE = \left(\frac{S.(A+B) S.(A-B)}{S.(A+E) S.(A-E)} \right)^{\frac{1}{2}} \times \frac{S.(A+B) S.(A-B)}{S.(A+F) S.(A-F)} \times 57.29$$

&c. $\times d$,

$$OK = \left(\frac{S.(A+B) S.(A-B)}{S.(A+F) S.(A-F)} \right)^{\frac{1}{2}} \times \frac{S.(A+B) S.(A-B)}{S.(A+E) S.(A-E)} \times 57.29$$

&c. $\times d$,

$$\frac{OK}{OE} = \left(\frac{S.(A+F) S.(A-F)}{S.(A+E) S.(A-E)} \right)^{\frac{1}{2}} \dots \dots \dots (A).$$

If the earth be a sphere, then $D=d$, and $E=F=B$; hence
 $OE=OK=57.29$, &c. $\times d$ (B).

If one of the places as B have no latitude, then B and E will be nothing, and F an arc corresponding to the $\cos. \frac{1}{D}$, the arc will not exceed six degrees, therefore less than A.

$$\text{Then } OE = \frac{\sin.^2 A}{\sin.(A+F) \sin.(A-F)} \times 57.29, \text{ \&c.} \times d,$$

$$OK = \frac{\sin. A}{(\sin.(A+F) \sin.(A-F))^{\frac{1}{2}}} \times 57.29, \text{ \&c.} \times d,$$

$$\frac{OK}{OE} = \frac{(\sin.(A+F) \sin.(A-F))^{\frac{1}{2}}}{\sin. A} \dots \dots \dots (C).$$

$$\frac{OK}{OE} = \frac{\left\{ \sin.(45^\circ+F) \cos.(45^\circ+F) \right\}^{\frac{1}{2}}}{\sin. 45^\circ} \dots \dots \dots (D).$$

If $A = 45^\circ$, and B less than A. Then

$$OE = \left(\frac{\sin.(45^\circ+B) \cos.(45^\circ+B)}{\sin.(45^\circ+E) \cos.(45^\circ+E)} \right)^{\frac{1}{2}} \times \frac{\sin.(45^\circ+B) \cos.(45^\circ+B)}{\sin.(45^\circ+F) \cos.(45^\circ+F)} \\ \times 57.29, \text{ \&c.} \times d.$$

$$OK = \left(\frac{\sin. (45^\circ + B) \cos. (45^\circ + B)}{\sin. (45^\circ + F) \cos. (45^\circ + F)} \right)^{\frac{1}{2}} \times \frac{\sin. (45^\circ + B) \cos. (45^\circ + B)}{\sin. (45^\circ + E) \cos. (45^\circ + E)} \\ \times 57.29, \&c. \times d,$$

$$\frac{OK}{OE} = \left(\frac{\sin. (A + F) \cos. (A + F)}{\sin. (45^\circ + E) \cos. (45^\circ + E)} \right)^{\frac{1}{2}} \dots \dots \dots (E).$$

If $A = 45^\circ$, and $B = 0$.

$$\text{Then } OE = \frac{\sin. 45^\circ}{\sin. (45^\circ + F) \cos. (45^\circ + F)} \times 57.29, \&c. \times d,$$

$$OK = \frac{\sin. 45^\circ}{\left\{ \sin. (45^\circ + F) \cos. (45^\circ + F) \right\}^{\frac{1}{2}}} \times 57.29, \&c. \times d,$$

COR. 1. If $s = 0$, then $c = 1$; we then have $OK = \frac{rS}{\sqrt{v^2 - C^2}}$,
 $OE = \frac{rS^2}{v^2 - C^2}$, and $\frac{OK^2}{OE^2} = \frac{v^2 - C^2}{S^2} = \frac{(v + C)(v - C)}{S^2}$.

COR. 2. Since $OE : OK :: S : \sqrt{v^2 - C^2}$, we then get
 $\frac{OE - OK}{OE} = 1 - \frac{\sqrt{v^2 - C^2}}{S} = 1 - \frac{\sqrt{(v + C)(v - C)}}{S}$.

COR. 3. Because $OE^2 : OK^2 :: S^2 : v^2 - C^2$, and $OE^2 : OE^2 - OK^2 :: S^2 : S^2 - (v - C^2) :: S^2 : 1 - v^2$.

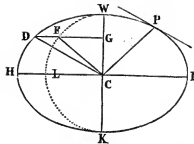
$$\text{Ther. } \frac{OE^2 - OK^2}{OE^2} = \frac{1 - v^2}{S^2} = \frac{(OE + OK)(OE - OK)}{OE^2},$$

$$\text{Or, } \frac{2OE(OE - OK)}{OE^2} = \frac{2(OE - OK)}{OE} = \frac{1 - v^2}{S^2}, \text{ nearly.}$$

$$\text{Ther. } \frac{OE - OK}{OE} = \frac{(1 + v)(1 - v)}{2S^2}, \text{ nearly.}$$

PROP. XIX.

To find the earth's axes, by having two degrees of a meridian measured, one at the equator, and the other in a given latitude.
 —(*Robertson's Navigation.*)



Let HI be the transverse, and KW the conjugate axis; P the given place on the meridian IWHK, and CD conjugate to CP, forming the angle DCW, equal to the latitude of P; on KW describe the circle WFLK, and draw DG parallel to HI, intersecting the circle in F, and join CF.

Put M, for the measure of a degree at the equator,

N, the measure of a degree at P,

A, to represent the angle GCF,

T, the nat. tang. lat. DCW, (radius unity),

t, the nat. tang. of A,

p = 57.29, &c. the degrees in the circular arc, equal to radius.

Then per trig. $CD : CF :: \sin. GFC : \sin. GDC :: \cos. GCF : \cos. GCD$.

But (Prop. VI.) $CD : CF (CW) :: \sqrt{N} \cdot \sqrt{M} :: \cos. A : \cos. \text{lat.}$

Ther. $\cos. \text{lat.} \times \sqrt{N} = \cos. A \times \sqrt{M} \therefore \cos. A = \left(\frac{N}{M} \right)^{\frac{1}{2}} \times \cos. \text{lat.}$

Hence the angle A is known.

Again (7. Ellip.) $GD : GF :: \text{tang. } GCD : \text{tang. } GCF :: T : t :: CH : CL :: CH : CW \therefore \frac{CW}{CH} = \frac{t}{T}$, a given ratio. (Cor. I.)

Prop. VI.) $p \times M = \frac{CW}{CH} \times CW = \frac{t}{T} \times CW \therefore CW = \frac{T}{t} \times pM$.

But $T \times CW = t \times CH \therefore CH = \frac{T}{t} \times CW = \frac{T^2}{t^2} \times pM$.

That is, $CW = \frac{\text{tang. lat.}}{\text{tang. A.}} \times pM$, and $CH = \left(\frac{\text{tang. lat.}}{\text{tang. A.}} \right)^2 \times pM$.

PROP. XX.

If D and d represent the lengths of a meridional degree in two given latitudes, the sines of which being S and s respectively, and $CK : CH :: 1 : 1+e$ (fig. Prop. XIX.) to determine an approximate value of e , and thence the ratio of the earth's axes.—(*Vince's Astronomy*, vol. ii.)

Let $CH = a$, and $CK = b$; then (Prop. XV.) $\frac{d}{D} = \left(\frac{a^2 - (a^2 - b^2) S^2}{a^2 - (a^2 - b^2) s^2} \right)^{\frac{1}{2}}$; and $a^2 : b^2 :: (1+e)^2 : 1$; or, $a^2 - b^2 : a^2 :: (1+e)^2 - 1 : (1+e)^2 :: 2e : 1+2e :: 1 : \frac{1}{2e} + 1 :: 1 : \frac{1}{2e}$. Ther. $(a^2 - b^2) \times \frac{1}{2e} = a^2$; that is, $a^2 - b^2 = 2ea^2$ (omitting e^2 , and considering $\frac{1}{2e} + 1 = \frac{1}{2e}$). Hence by substitution, $\frac{d}{D} = \left(\frac{a^2 - 2ea^2 S^2}{a^2 - 2ea^2 s^2} \right)^{\frac{1}{2}} = \left(\frac{1 - 2e S^2}{1 - 2e s^2} \right)^{\frac{1}{2}} = \left(\frac{1 - e S^2}{1 - e s^2} \right) = \frac{1 - 3e S^2}{1 - 3e s^2}$, nearly. From which equation $e = \frac{D-d}{3(S^2 D - s^2 d)}$.

But $CK : CH :: 1 : 1+e :: \frac{1}{e} : \frac{1}{e} + 1$; that is, $CK : CH :: \frac{3S^2 D - 3s^2 d}{D-d} : \frac{3S^2 D - 3s^2 d}{D-d} + 1$ nearly the required ratio (a).

If $CH : CK :: 1 : m :: 1+e : 1$ (by the preceding). Then $m \times (1+e) = 1 \therefore me = 1 - m$; or $1 : m :: e : 1 - m$. But, on account of CH being nearly equal to CK , we may consider m nearly equal to unity; and therefore $e = 1 - m = \frac{D-d}{3(S^2 D - s^2 d)}$
 $\therefore m = 1 - \frac{D-d}{3S^2 D - 3s^2 d} = 1 - \frac{r}{w}$.

But $CH : CK :: 1 : m :: 1 : 1 - \frac{r}{w} :: w : w - r :: \frac{w}{r} : \frac{w}{r} - 1$.

Ther. $CH : CK :: \frac{3DS^2 - 3s^2d}{D-d} : \frac{3S^2D - 3s^2d}{D-d} - 1$, nearly (b).

COR. 1. If d be the measure of a meridional degree at the equator, then $s=0$.

And (a) $CK : CH :: \frac{3S^2D}{D-d} : \frac{3S^2D}{D-d} + 1$.

COR. 2. By supposing d and s , as in corollary 1.

Then (b) $CH : CK :: \frac{3S^2D}{D-d} : \frac{3S^2D}{D-d} - 1$.

COR. 3. If $s=0$, then by the proposition $D : d :: 1 : 1 - 3S^2e$, from whence $D = \frac{d}{1 - 3S^2e} = d(1 + 3S^2e)$ nearly.

COR. 4. Since $D = d + 3deS^2$; or $D - d = 3deS^2$, we shall have $D - d$ as S^2 , because $3de$ is given; that is, the degrees of the meridian from the equator towards the poles are increased in a duplicate ratio of the sine of latitude nearly.

PROP. XXI.

To render the expression $\frac{3S^2D - 3s^2d}{D-d}$, as determined by Prop. XX., applicable to the use of logarithms. $\frac{3S^2D - 3s^2d}{D-d} =$
 $(DS^2 - d^2) \times \frac{3}{D-d} = (1 - \frac{d^2}{DS^2}) \times \frac{3DS^2}{D-d} = \left\{ \left(1 + \frac{s}{S}\sqrt{\frac{d}{D}}\right) \right.$
 $\left. \left(1 - \frac{s}{S}\sqrt{\frac{d}{D}}\right) \right\} \times \frac{3DS^2}{D-d} = \sin.(90^\circ + A) \sin.(90^\circ - A) \times \frac{3DS^2}{D-d} =$
 $\frac{\cos.^2 A \times S^2 \times 3D}{D-d}$. $A =$ an arc corresponding to the $\sin. \frac{s}{S}\sqrt{\frac{d}{D}}$;
 an expression very convenient for logarithms.

COROLLARY. The expression in Cor. 3. Prop. XX. may be reduced as follows:

$$D = \frac{d}{1 - 3eS^2} = \frac{d}{(1 + S\sqrt{3e})(1 - S\sqrt{3e})} = \frac{d}{\cos.^2 B}$$

$B =$ an arc corresponding to the $\sin S\sqrt{3e}$.

PROP. XXII.

In a given ellipse, to find an approximate value for the radius of curvature in a given latitude.

Put a = semi-transverse diameter,

b = semi-conjugate, $a^2 - b^2 = c^2$,

S = sine of latitude, and

R = radius of curvature in the given latitude.

$$\text{Then Prop. XV. } R = \frac{a^2 b^2}{(a^2 - (a^2 - b^2) S^2)^{\frac{3}{2}}}.$$

But $b^2 = a^2 - 2ac + c^2 = a^2 - 2ac \therefore a^2 - b^2 = 2ac$ (omitting c^2).

$$\begin{aligned} \text{Then by substitution } R &= \frac{a^2 b^2}{(a^2 - 2ac S^2)^{\frac{3}{2}}} = \frac{a^2 b^2}{(a - c S^2)^3} = \\ \frac{a^2 b^2}{a^3 - 3a^2 c S^2} &= \frac{b^2}{a - 3c S^2} = \frac{a^2 - 2ac}{a - 3c S^2} = \frac{a - 2c}{1 - \frac{3c}{a} S^2} = a - 2c + \end{aligned}$$

$3c S^2$, nearly, omitting c^2 &c. which is P. Frif's Rule. See *Gentleman's Diary*, 1806.

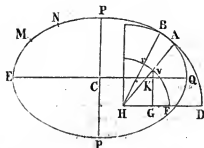
$$\text{COR. } 1 - \frac{3c}{a} S^2 = (1 + S\sqrt{\frac{3c}{a}})(1 - S\sqrt{\frac{3c}{a}}); \text{ find an arc } A,$$

corresponding to the sin. $S\sqrt{\frac{3c}{a}}$; then $R = \frac{a - 2c}{\cos^3 A}$.

PROP. XXIII.

To determine the ratio of the earth's axes from the measures of convenient portions of a meridian in any two given latitudes; the earth being supposed a spheroid generated by the rotation of an ellipse upon its minor axis. *Doct. Gregory's Trig.*

Let the ellipse $PEpQ$ represent a terrestrial meridian passing through the poles P, p , and cutting the equator in E, Q ; C the center, CQ the radius of the equator, and PC half the polar axis.



Let AB be an indefinitely small arc of the meridian, whose radius of curvature is AH ; join HB ; draw HD parallel to EQ ; on the center H , and with the radius $HF = 1$, describe the circular arc Fv , and draw the sine vG ; also on the center H , and with the radius of curvature HA , describe the circular arc DAB .

Let $CQ = a$, $CP = b$, $a - b = c$, $S = vG = \sin. \text{lat.} = \sin. \text{angle } AKQ = AHD$; $\phi = \text{circular arc } Fv$, and $\partial\phi = vr$; $z = \text{elliptic arc, } QA$, and $\partial z = AB$. Then per similar sectors, $Hv : vr :: HA : AB$, that is, $1 : \partial\phi :: HA : \partial z$, ther. $\partial z = \partial\phi \times HA$; but Prop. XXII. $HA = a - 2c + 3cS^2$ nearly, ther. $\partial z = \partial\phi (a - 2c + 3cS^2) = (a - 2c) \partial\phi + 3cS^2 \partial\phi$; but $S^2 = \frac{1}{2}(1 - \cos. 2\phi)$, ther. $\partial z = (a - 2c) \partial\phi + \frac{3c}{2} \partial\phi - \frac{3c}{2} \cos. 2\phi \partial\phi$. By integration $z = (a - \frac{c}{2}) \phi - \frac{3c}{4} \sin. 2\phi = a\phi - \frac{c}{2} (\phi + \frac{1}{2} \sin. 2\phi)$, an expression which needs no correction.

Let MN be an arc of the elliptic meridian,

ϕ' the latitude of M , one of its extremities,

ϕ'' that of N , the other extremity; we have

$$EM = a\phi' - \frac{c}{2} (\phi' + \frac{1}{2} \sin. 2\phi')$$

$$EN = a\phi'' - \frac{c}{2} (\phi'' + \frac{1}{2} \sin. 2\phi'')$$

And their difference $EN - EM$, that is,

$$MN = a(\phi'' - \phi') - \frac{c}{2} \left\{ (\phi'' - \phi') + \frac{1}{2} (\sin. 2\phi'' - \sin. 2\phi') \right\}.$$

In which equation a and c are the only unknown quantities. In like manner by the measurement of another arc of the meridian, another equation will be obtained, in which a and c are the only unknown quantities. Hence the values of a and c become known, from which the axes may be determined.

Thus. If l = length of an arc measured,

$$m = \phi'' - \phi' = \text{co-efficient of } a,$$

$$n = \frac{1}{2} \{ (\phi'' - \phi') + \frac{1}{2} (\sin. 2\phi'' - \sin. 2\phi') \} = \text{co-efficient of } c,$$

And if l' = length of another arc,

$$m' = \text{co-efficient of } a, \text{ and}$$

$$n' = \text{co-efficient of } c; \text{ then we shall have}$$

$$ma - nc = l, \text{ and } m'a - n'c = l'; \text{ whence } a = \frac{n'l - n'l'}{m'n' - m'n}, c = \frac{m'l - m'l'}{m'n' - m'n}, \text{ and } \frac{c}{a} = \frac{m'l - m'l'}{n'l - n'l'}.$$

$$\text{It is also evident that } c = \frac{ma - l}{n} = \frac{m'a - l'}{n'}, \text{ and } b = a - c.$$

PROP. XXIV.

A degree of the earth's equator is the first of two mean proportionals between the *last* and first degrees of latitude.

Let R and r represent the radii of curvature corresponding to a degree of latitude at the poles and at the equator, and CE the radius of the equator.

$$\text{We have to prove that } CE = \sqrt[3]{rR}.$$

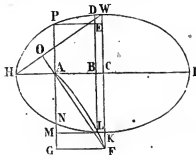
$$\text{Per Cor. 1 and 2, Prop. VI. } R = \frac{CE^3}{CP}, \text{ and } r = \frac{CP^3}{CE}.$$

$$\text{Then } \sqrt[3]{rR} = \sqrt[3]{\frac{CP^3}{CE} \times \frac{CE^3}{CP}} = \sqrt[3]{CE^3} = CE, \text{ as required.}$$

PROP. XXV.

If A be the center of curvature at H , the vertex of the transverse axis, and F , the center of curvature at W , the vertex of the

conjugate axis, and AF and HW be joined; the right-angled triangles HCW, ACF, will be similar.



By Cor. 1. and 2. Prop. VI. $HA = \frac{CW^2}{HC}$, and $WF = \frac{HC^2}{CW}$,
 ther. $HC - HA = AC = HC - \frac{CW^2}{HC} = \frac{HC^2 - CW^2}{HC}$; and $WF - WC = CF = \frac{HC^2}{CW} - CW = \frac{HC^2 - CW^2}{CW}$. Hence it will be,
 as $AC : CF :: \frac{HC^2 - CW^2}{HC} : \frac{HC^2 - CW^2}{CW} :: CW : CH$.

Therefore Def. 1. 6 : E. the triangles HCW, ACF are similar.

COROLLARY.

By producing FA to O, the triangles AOH, ACF will be similar, and FO at right angles to HW.

PROP. XXVI.

If the evolute ALF of the elliptic arc HPW intersect the ellipse in L, and the rectangle ACFG be completed, to determine the ordinate LM parallel to CH, when CF is greater than the semi-conjugate CK.

Produce GA to P; draw PE parallel, and LD perpendicular to HI. By Cor. 1. Prop. VI. $HA = \frac{CW^2}{HC}$. $\therefore AI = \frac{2CH^2 - CW^2}{CH}$,

By Cor. 1. Prop. VI. $HA = \frac{b^2}{a}$,

And Prop. XV. $LP = \frac{a^2 b^2}{(a^2 - v^2 s^2)^{\frac{3}{2}}} = \frac{a^2 b^2}{(b^2 + v^2 c^2)^{\frac{3}{2}}}$

Per trig. $PN = \frac{a^2 b^2 s}{(a^2 - v^2 s^2)^{\frac{3}{2}}}$, and $LN = \frac{a^2 b^2 c}{(b^2 + v^2 c^2)^{\frac{3}{2}}}$.

But $PN - PT = TN = AM$, and $LN + TH - HA = LM$.

That is, $\frac{a^2 b^2 s}{(a^2 - v^2 s^2)^{\frac{3}{2}}} - \frac{b}{a} \sqrt{2ax - x^2} = AM$,

And $\frac{a^2 b^2 c}{(b^2 + v^2 c^2)^{\frac{3}{2}}} - \frac{b^2}{a} + x = ML$.

COROLLARY 1.

When the angle PLN becomes 90 degrees, then $s=1$, $c=0$, $PT=CW=b$, $HT=HC=a$, $AM=CF$, and $LM=FG$. The two preceding expressions will then become $\frac{a^2}{b} - b = \frac{a^2 - b^2}{b} = CF$, and $a - \frac{b^2}{a} = \frac{a^2 - b^2}{a} = FG$. The same as determined in Prop. XXV.

COROLLARY 2.

If the angle PLN become nothing, then $s=0$, $c=1$, and $HT=x=O$; when this is the case, both AM and ML become nothing.

COROLLARY 3.

The length of the whole evolute $ALF = FW - AH = \frac{a^2}{b} - \frac{b^2}{a} = \frac{a^2 - b^2}{ab}$.

COROLLARY 4.

The length of any part of the evolute $AL = LP - AH = \frac{a^2 b^2}{(a^2 - v^2 s^2)^{\frac{3}{2}}} - \frac{b^2}{a} = \left\{ \frac{a^2}{(a^2 - v^2 s^2)^{\frac{3}{2}}} - \frac{1}{a} \right\} b^2$.

$$CI^2 - CK^2 : CI^2, \text{ ther. } QK = \frac{CK \times CI^2}{CI^2 - CK^2} = \frac{n m^2}{m^2 - n^2} = \frac{n m^2}{v};$$

by Prop. XXXVII. Ellip. $PQ = \frac{m^2}{\sqrt{m^2 + n^2 t^2}}; (t = \text{tang. } KPQ);$

Then per trig. $PQ : QK :: \text{rad.} : \text{tang. } KPQ.$ That is,

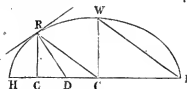
$$\frac{m^2}{\sqrt{m^2 + n^2 t^2}} : \frac{n m^2}{v} :: 1 : t; \text{ ther. } \frac{t^2}{m^2 + n^2 t^2} = \frac{n^2}{v^2}, \text{ or } t =$$

$$\frac{m n}{\sqrt{v^2 - n^4}} = \frac{m n}{\sqrt{(m^4 - 2 m^2 n^2 + n^4 - n^4)}} = \frac{n}{\sqrt{m^2 - 2 n^2}} =$$

$$\frac{CK}{\sqrt{CI^2 - 2 CK^2}}. \text{ Hence } KP = \frac{CI^2}{\sqrt{(CI^2 - 2 CK^2)}}.$$

EXAMPLE 2.

If the earth be an oblate spheroid, the ratio of whose axes is 230 to 229, in what latitude will the line of motion, in which a heavy body falls to the earth, make the greatest angle with one drawn perpendicular to the surface, and how much is that angle?—*Lady's Diary*, 1806.



Let H W I represent half the elliptic meridian passing through the required latitude R; H I the equatorial, and C W half the polar axis, and join I W. Then by Proposition XL. Ellip. we have the following construction and computation.

CONSTRUCTION.

Draw C R parallel to I W, and draw the normal R D, and D R C will be the required angle.

COMPUTATION.

$$\text{Tang. } DRC = \frac{CI^2 - CW^2}{2 CI \times CW} = \frac{CI + IW}{2 CI \times CW} = (CI - CW = 1)$$

$$\frac{230+229}{2 \times 230 \times 229} = \frac{459}{105340} = \frac{1}{229.5}, \text{ corresponding to } 14'.56''\frac{1}{2}.$$

But the angles GRC and GRD are complements to each other; therefore $90^\circ - CRG = GRD = 90^\circ - (CRD + DRG)$, that is, $2GRD = 90^\circ - CRD$; or $GRD = 45^\circ - \frac{1}{2}CRD$, therefore $90^\circ - GRD = GDR = 90^\circ - 45^\circ + \frac{1}{2}CRD = 45^\circ + \frac{1}{2}CRD = 45^\circ . 7' . 29'' . 22''\frac{1}{2}$, the required latitude.

EXAMPLE 3.

To determine a place on the earth, where a degree of the meridian is equal to a degree of the equator; the ratio of the axis to the equatorial diameter being that of 229 to 230.—*Lady's Diary*, 1802.

Put $230=a$, $229=b$, $a^2-b^2=v^2$, S = nat. sin. of the required latitude, and R the radius of curvature of the meridian in the proposed latitude.

Then by Prop. XV. $R = \frac{a^2 b^2}{(a^2 - v^2 S^2)^{\frac{3}{2}}}$; but the lengths from the degrees being as their respective radii of curvature, and from the conditions of the question, we have $\frac{a^2 b^2}{(a^2 - v^2 S^2)^{\frac{3}{2}}} = a$; from

$$\text{whence } S^2 = \frac{a^2 - (a b^2)^{\frac{2}{3}}}{a^2 - b^2} = \frac{a^2 - (a b^2)^{\frac{2}{3}}}{a+b} = (a-b=1) \frac{306}{459} \therefore$$

$\text{Log. } S = \text{Log. } \sqrt{\frac{306}{459}} = \bar{1}.9119544$, corresponding to $54^\circ . 44' . 8''$, the required latitude.

EXAMPLE 4.

Given the earth's axes, 7977 and 7940 miles, to determine, by a simple and accurate process, the radius of curvature in apparent latitude $50^\circ . 23'$.—*Gentleman's Diary*, 1805.

Put $7977=a$; $7940=b$, $a^2-b^2=v^2$, and nat. sin. $50^\circ . 23'=S$; then (Prop. XV.) $2R = \frac{a^2 b^2}{(a^2 - v^2 S^2)^{\frac{3}{2}}} = \frac{63632529 \times 63043600}{(63283059)^{\frac{3}{2}}} =$

7968.9. Ther. $R = \frac{7968.9}{2} = 3984.45 =$ the required radius of curvature.

In Prop. XV. a and b represent the semi-axes; but in this example they represent the whole axes; ther. $2R$ is used instead of R .

EXAMPLE 5.

To find in what latitude a degree of the meridian is equal in length to two degrees of longitude in the same latitude, the earth being considered as an oblate spheroid, the axes of which are as 229 to 230.—*Lady's Diary*, 1810.

Put $230=a$, $229=b$, $a^2-b^2=v^2$; $S, C, T=\sin. \cos.,$ and tang. of the required latitude; R =radius of curvature of the meridian, and r =radius corresponding to a degree of longitude.

By Prop. XXXVII. $r = \frac{a^2}{\sqrt{a^2+b^2} T^2}$, by Prop. XV. $R = \frac{a^2 b^2}{(b^2+v^2 C^2)^{\frac{3}{2}}}$. But from the lengths of the degrees being as their respective radii of curvature, and from the condition of the question, we have $\frac{a^2 b^2}{(b^2+v^2 C^2)^{\frac{3}{2}}} = \frac{2 a^2}{(a^2+b^2 T^2)^{\frac{3}{2}}}$. But $a^2+b^2 T^2 = a^2 + \frac{b^2 S^2}{C^2} = \frac{a^2 C^2 + b^2 (1-C^2)}{C^2} = \frac{b^2 + (a^2-b^2) C^2}{C^2} = \frac{b^2+v^2 C^2}{C^2}$; ther. $\frac{b^2}{(b^2+v^2 C^2)^{\frac{3}{2}}} = \frac{2}{C (b^2+v^2 C^2)^{\frac{3}{2}}}$, or $\frac{b^2}{(m^2)^{\frac{3}{2}}} = \frac{2 C}{(m^2)^{\frac{3}{2}}}$ that is $\frac{b^2}{m^2} = \frac{2 C}{m}$ $\therefore 2 C m^2 = b^2$; or $2 C \times (b^2+v^2 C^2) = b^2$; ther. $v^2 C^2 + b^2 C = \frac{b^2}{2}$. In a sphere $V^2=0$; $\therefore C = \frac{1}{2} = \cos. 60^\circ$. But if, instead of the $\cos. C$, we substitute its equal $\frac{1}{\sec. \phi} = \frac{1}{\phi}$, the above equation will become $\frac{v^2}{\phi^2} + \frac{b^2}{\phi} = \frac{b^2}{2}$ $\therefore \phi^2 - 2 \phi^2 = \frac{2 v^2}{b^2} = \frac{2(a^2-b^2)}{b^2} = \frac{a+b}{b^2} \times 2(a-b=1)$; ther. $(\phi-2) \times \phi^2 = \frac{918}{52441}$

lium to Prop. XIV. Ellip. we have $H z \times z I : P z \times z Z :: C I^2 :$

$$C F^2 = \frac{C H^2 \times C K}{c^2 (C K^2 + t^2 \cdot C H^2)} \text{ (ibid.) } c = \cos, t = \text{tang. } H C F = P z I = 70^\circ . 22' . 18'' = (5.6716)^2 \therefore z Z = \frac{H z \times z I \times C F^2}{P z \times C I^2} = 5.414.$$

Therefore $P z + z Z = P Z = 9.132$; and $P V = V Z = 4.566$.

Again per Scholium to Prop. XIV. Ellip. we have $q V \times V g : P V \times V Z :: C I^2 : C F^2 \therefore q V \times V g = \frac{P V \times V Z \times C I^2}{C F^2} = \frac{P V^2 \times C I^2}{C F^2}$, but from the nature of the circle, $q V \times V g =$ square

of the ordinate corresponding to the point V, or in this example to the square of the semi-transverse axis of the elliptic section $t Z s P$; ther. $V t = V s = \sqrt{\frac{P V^2 \times C I^2}{C F^2}} = 6.4405$, and thence

the transverse $s t = 12.881$, whose conjugate axis is $P Z$. In the triangle $C V z$ we have $P V - P z = V z = 0.748$, $C z = 4.894$ and the angle $C z V = 70^\circ . 22' . 18''$, to find $C V = 4.7318$; and Prop.

XLV. Ellip. $C p = \frac{C V \times C I}{\sqrt{C I^2 - (V s)^2}} = 7.9769$, hence $V h = 12.709$

and $V p = 3.245$. And from Dr. Hutton's Mensuration,

$$\left. \begin{array}{l} \text{The area of the section } P t Z s = 92.368 \\ \text{Solidity of greater segment } Z H W P = 1316.3 \\ \text{Ditto - - less segment } Z p I P = 158.2 \\ \text{Whole spheroid - - - - -} = 1474.5 \end{array} \right\} \text{ inches.}$$

EXAMPLE 7.

In latitude $50^\circ . 41'$ north the length of a degree on the meridian is 60851 fathoms, and the measure of a degree perpendicular to the meridian is 61182 fathoms, to find the earth's axes.—*Trig. Survey*, vol. i. p. 309.

Put $s = \text{nat. sin. } 50^\circ . 41'$, $m = 60851$, $p = 61182$, and $d = 57.29$, &c. the degrees in a circular arc equal to radius. Let $H =$ an arc corresponding to the nat. sin. of $s \sqrt{\frac{m}{p}}$; then (cor. 3. Prop. XVI.)

$$d \sqrt{p m} \times \frac{\cos.^2 \text{ lat.}}{\cos.^2 H} = \frac{1}{2} \text{ the polar axis,}$$

$$d p \times \frac{\cos. \text{ lat.}}{\cos. H} \dots = \frac{1}{2} \text{ the equatorial axis;}$$

$$\text{Log. } d = 57.29, \&c. \dots = 1.7581226$$

$$\text{Log. } \sqrt{p m} = \sqrt{(61182 \times 60851)}. \dots = 4.7854457$$

$$2 \log. \cos. 50^\circ.41'. \dots = 1.6036384$$

$$6.1472067$$

$$\text{Log. } \sqrt{\frac{m}{p}} = \sqrt{\frac{60851}{61182}} \dots = 1.9985220$$

$$\text{Log. } \sin. 50^\circ.41' \dots = 1.8885479$$

$$\text{Log. } \sin. \text{ of } H \dots = 1.8873699$$

$$2 \log. \cos. \text{ of } H, \text{ subtract.} \dots = 1.6071274$$

$$\text{Diff.} = \log. 3465002 \text{ fathoms} = \frac{1}{2} \text{ polar axis} = 6.5400793$$

$$\text{Log. } d \dots = 1.7581226$$

$$\text{Log. } p = 61182. \dots = 4.7866237$$

$$\text{Cos. lat.} \dots = 1.8018192$$

$$6.3465655$$

$$\text{Log. } \cos. \text{ of } H, \text{ subtract} \dots = 1.8035637$$

$$\text{Diff.} = 3491417 \text{ fathoms} = \frac{1}{2} \text{ equatorial axis} = 6.5430018$$

EXAMPLE 8.

Having at the same point the length of a degree on the meridian 60850 fathoms, and also that of a degree perpendicular to the meridian 61182 fathoms, to find the length of a degree forming an angle with the meridian equal to $81^\circ.56'.53''$.—*Lady's Diary*, 1801.

Put $p = 61182$, $m = 60850$, and $s = \text{nat. sin. } 81^\circ.56'.53''$.
Then (Cor. 2. Prop. XVII.)

$$\text{Log. } (p-m) = 332 \quad = 2.5211331$$

$$\text{Log. } p = 61182 \quad = 4.7966237$$

$$\text{Log. } \frac{p-m}{p} \quad . . \text{ Subtract} \quad = \underline{\underline{3.7345144}}$$

$$\text{Log. } \sqrt{\frac{p-m}{p}} \quad = \underline{\underline{2.8672572}}$$

$$\text{Log. sin. } 81^{\circ}.56'.53'' \quad . . \text{ Add} \quad . . = \underline{\underline{1.9956973}}$$

$$\text{Log. sin. of an arc } A \quad = \underline{\underline{2.8629545}}$$

$$2 \text{ log. cos. of } A \quad = \underline{\underline{1.9976834}}$$

$$\text{Log. } m = 60850 \quad = \underline{\underline{4.7842606}}$$

$$\text{Diff.} = \text{log. } 61175.45 \quad = \underline{\underline{4.7865772}}$$

Therefore the length of the required oblique degree is 61175.45 fathoms.

EXAMPLE 9.

In latitude $51^{\circ}.28'.40''$ N. the measure of a degree on the meridian is 60868 fathoms, and in latitude $51^{\circ}.5'$ N. the length of a meridional degree is 60859 fathoms; required the earth's axes.—*Mathematical Repository*, No. 14.

Then (A) Prop. XVIII.

$$\text{Log. } \sqrt{\frac{d}{D}} = \text{log. } \sqrt{\frac{60844\frac{1}{2}}{60859}} \quad . . . = \underline{\underline{1.9999786}}$$

$$\text{Log. sin. } B = 51^{\circ}.5' \quad = \underline{\underline{1.8910133}}$$

$$\text{Log. sin. } E = 51^{\circ}.4'.47''.24''' \quad . . = \underline{\underline{1.8909919}}$$

$$\text{Log. } \sqrt{\frac{d}{D}} \quad = \underline{\underline{1.9999786}}$$

$$\text{Log. cos } 51^{\circ}.5' \quad = \underline{\underline{1.7980906}}$$

$$\text{Log. cos. } F = 51^{\circ}.5'.8''.11''' \quad . . = \underline{\underline{1.7980692}}$$

$$\text{Log. sin. } A+B = 77^{\circ}. 26'. 20''. 0''' = 9.9894786$$

$$\text{Log. sin. } A-B = 0. 23. 40. 0 = 7.8378598$$

$$\text{Ar. comp. } A+E = 102. 33. 27. 24 = 0.0105155$$

$$\text{Ar. comp. } A-E = 0. 23. 52. 36 = 2.1583037$$

$$2) 19.9961576$$

$$9.9890788$$

$$A+B = 9.9894786$$

$$A-B = 7.8378598$$

$$\text{Ar. comp. } A+F = 102. 33. 48. 11 = 0.0105253$$

$$\text{Ar. comp. } A-F = 0. 23. 31. 49 = 2.1646502$$

$$57. 29, \&c. = 1.7581226$$

$$d = 60859 = 4.7843248$$

$$OE = 3491725 = 6.5430401$$

$$\text{Log. sin. } A+B = 9.9894786$$

$$\text{Log. sin. } A-B = 7.8378598$$

$$\text{Ar. comp. } A+F = 0.0105253$$

$$\text{Ar. comp. } A-F = 2.1646502$$

$$2) 0.0025139$$

$$0.0012569$$

$$A+B = 9.9894786$$

$$A-B = 7.8378598$$

$$\text{Ar. comp. } A+E = 0.0105155$$

$$\text{Ar. comp. } A-E = 2.1583037$$

$$57. 29, \&c. = 1.7581226$$

$$d = 4.7843248$$

$$OK = 3466266 = 6.5398619$$

$$\text{Log. sin. } A+F = 9.9894747$$

$$\text{Log. sin. } A-F = 7.8353498$$

$$\text{Ar. comp. } A+E = 0.0105155$$

$$\text{Ar. comp. } A-E = 2.1583037$$

$$2) 19.9936437$$

$$\frac{OK}{OE} = 0.9927086 \dots = \underline{9.9968218}$$

$$OK : OE :: 0.9927086 : 1 :: 231 : 232.696$$

$$OK : OE :: 1 : 1.0073449 :: 231 : 232.696$$

Or $OK \div OE$ may be thus:

$$\text{From log. } OK \dots = 6.5398619$$

$$\text{Take log. } OE \dots = \underline{6.5430401}$$

$$\text{Remain same logarithm as above} \dots = \underline{\underline{1.9968218}}$$

EXAMPLE 10.

In latitude $66^\circ.20'$ N. the measure of a degree on the meridian is 57438 toises, and the measure of a degree at the equator is 56757 toises, to find the earth's axes.—*Robertson's Navigation*.

ARTICLE (C) PROP. XVIII.

$$\text{Log. } d = 56757 \dots = 4.7530194$$

$$\text{Log. } D = 57438 \dots = \underline{4.7591993}$$

$$3) \underline{1.9938201}$$

$$\text{Cos. } F = 5^\circ.34'.34'' \dots = \underline{1.9979400}$$

$$A = 66.20.0$$

$$\underline{71.54.34 = A + F}$$

$$\underline{60.45.26 = A - F}$$

$$\text{Log. sin. } A + F \dots = 9.9779827$$

$$\text{Log. sin. } A - F \dots = \underline{9.9407941}$$

$$2) \underline{19.9187768}$$

$$\text{Log. } (S. (A + F) S. (A - F))^{\frac{1}{2}} = 9.9593884 \text{ (a)}$$

$$\text{Sin. } A, \text{ subtract} \dots = \underline{9.9618463}$$

$$\text{Log. } \frac{C W}{C H} = 0.9943565 \dots = \underline{\underline{1.9975421}}$$

Log. sin. A	=	9.9618463
Log. 57.29; &c.	=	1.7581226
Log. d	=	4.7530194
		<u>16.4729883</u>
Log. (a)	=	9.9593894
Log. C W in toises	=	6.5135999
Add*		0.0276553
Log. C W = 3477405 fath.	=	<u>6.5412552</u>
2 log. A	=	19.9236926
Log. 57.29, &c.	=	1.7581226
Log. d	=	4.7530194
		<u>26.4348346</u>
2 log. (a)	=	19.9187768
Log. C H in toises	=	6.5160578
Add		0.0276553
Log. C H = 3497140 fath.	=	<u>6.5437131</u>

* Fath. : Toise :: 6 : 6.3945. Doctor Hutton's Dictionary.

Ther. Fath. $\times 6 =$ Toise $\times 6.3945$.

Or Fath. $= \frac{6.3945}{6} \times$ Toise,

Toise $= \frac{6}{6.3945} \times$ Fath.

Log. $\frac{6.3945}{6}$ = 0.0276553

Log. $\frac{6}{6.3945}$ = 1.9723447

SAME EXAMPLE, BY PROP. XIX.

Log. 57438	= 4.7591993
Log. 56757	= 4.7530194
	<u>3) 0.0061799</u>
	0.0020599
Log. cos. 66°. 20'	= 9.6035936
Cos. A=66°. 12'. 50".	= 9.6056535
Log. tang. A	= 10.3557948
Log. tang. 66°. 20'	= 10.3582527
Log. $\frac{C W}{C H}$	= 1.9975421
Tang. lat.	= 10.3582527
Log. 57.29, &c.	= 1.7581226
Log. 56757	= 4.7530194
	<u>16.8693947</u>
Log. tang. A	= 10.3557948
Log. C W, in toises	= 6.5135999
2 tang. lat.	= 20.7165054
Log. 57.29, &c.	= 1.7581226
Log. 56757	= 4.7530194
	<u>27.2276474</u>
2 log. tang. A	= 20.7115896
Log. C H, in toises	= 6.5160578

Each of the preceding methods brings out exactly the same answers, although the principles from whence they are derived are different.

EXAMPLE 11.

If a = half the earth's equatorial diameter, and b = half the polar axis, and $\frac{a-b}{a} = \frac{1}{250}$; to find the ratio of b to a .

From the given equation we have $(300-1) \times a = 300 \times b$. Therefore $b : a :: 299 : 300 :: 1 : \frac{300}{299} :: 1 : 1 + \frac{1}{299} :: 1 : 1 + 0.0033445$.

EXAMPLE 12.

Given the earth's compression $\frac{1}{250}$, and the measure of a degree of latitude at the equator 56747 toises, to find the length of a meridional degree in latitude 30° .—*Vince's Astronomy*, vol. ii. page 110.

By Cor. 3. Prop. XX. $D = \frac{d}{1 - 3eS^2}$, where $d = 56747$, $3e = \frac{1}{250}$ (exam. 11.), and $S^2 = \frac{1}{4}$. Therefore $D = \frac{56747}{1 - \frac{3}{1196}} =$

$\frac{1196 \times 56747}{1193} = \frac{67869412}{1193} = 56889$ toises, the required length of the meridional degree.

EXAMPLE 13.

From the data given in Example 9th, to find the ratio of the earth's diameters by Prop. XXI.

$S = \sin. 51^\circ. 28'. 40'' - \log. = \bar{1}.8934103$
 $s = \sin. 51. 5. 0 - \log. = \bar{1}.8910133$
 $D = 60868$ fathoms - - - $\log. = 4.7843890$
 $d = 60859$ fathoms - - - $\log. = 4.7843248$
 $D - d = 9$ do. ar. com. - $\log. = \bar{1}.0457575$. A. C.
 - - - - - $\log. 3 = 0.4771213$

$A =$ an arc corresponding to the $\sin. \frac{s}{S} \sqrt{\frac{d}{D}}$,

And $\frac{3S^2D - 3s^2d}{D - d} = \frac{\cos.^2 A \times S^2 \times 3D}{D - d}$.

First to find the arc A.

$$\text{Log. } d \dots\dots\dots = 4.7843248$$

$$\text{Log. } D. \text{ ar. comp.} \dots\dots\dots = \overline{5.2156110}$$

$$2) \overline{1.9999358}$$

$$\text{Log. } \sqrt{\frac{d}{D}} \dots\dots\dots = \overline{1.9999679}$$

$$\text{Log. } s \dots\dots\dots = \overline{1.8910133}$$

$$\text{Log. } S. \text{ ar. comp.} \dots\dots\dots = \overline{0.1065897}$$

$$\text{Log. sin. } A = 83^\circ.56'.44'' \dots\dots\dots = \overline{1.9975709}$$

To find $\frac{3S^2D - 3s^2d}{D-d}$.

$$\text{Log. cos.}^2 A \dots\dots\dots = \overline{2.0462862}$$

$$\text{Log. } S^2 \dots\dots\dots = \overline{1.7868206}$$

$$\text{Log. } 3 \dots\dots\dots = 0.4771213$$

$$\text{Log. } D \dots\dots\dots = 4.7843890$$

$$\text{Log. } D-d, \text{ ar. comp.} \dots\dots\dots = \overline{1.0457575}$$

$$\text{Log. } 138.16 \dots\dots\dots = \overline{2.1403746}$$

Hence CK : CH :: 138.16 : 139.16 :: 231 : 232.672.

And CH : CK :: 138.16 : 137.16 :: 232.696 : 231.011.

Which very nearly agrees with Example 9th.

EXAMPLE 14.

Given the earth's compression $\frac{1}{289}$, and the measure of a degree of latitude at the equator 56747 toises, to find the length of a meridional degree in latitude 73° , by Cor. to Prop. 21.

$$D = \frac{d}{\cos^2 B} = \frac{56747}{\cos^2 B}; B = \sqrt{\frac{1}{289}} \times \sin. 73^\circ.$$

$$\text{Log. } 3 \dots\dots\dots = 0.4771213$$

$$\text{Log. } 299. \text{ ar. comp.} \dots\dots\dots = \overline{3.5243288}$$

$$2) \overline{2.0014501}$$

$$\overline{1.0007250}$$

$$\text{Log. sin. } 73^\circ \dots\dots\dots = \overline{1.9805963}$$

$$\text{Log. sin. } 5^\circ.29'.48'' \dots\dots\dots = \overline{2.9813213}$$

$$\text{Cos. } 5^{\circ} . 29' . 48'' \quad = \bar{1} \cdot 9979984$$

2

$$\bar{1} \cdot 9959968$$

$$\text{Ar. comp.} \quad = 0 \cdot 0040032$$

$$\text{Log. } 56747 \quad = 4 \cdot 7539429$$

$$\text{Log. } 57272 \cdot 5 \quad = 4 \cdot 7579461$$

Therefore the length of a meridional degree } = 57272 \cdot 5 \text{ toises}

in lat. 73° }

By actual multiplication and division . . . = 57272 \cdot 5194

By Vince's Astronomy, vol. ii. page 110 . . = 57269

EXAMPLE 15.

From the data given in Example 4th to find the radius of curvature, by Cor. to Prop. 22nd.

$$R = \frac{a-2c}{\cos^2 A}; \quad a=7977, \quad b=7940, \quad a-b=c=37,$$

A=an arc, corresponding to $S\sqrt{\frac{3c}{a}}$.

$$\text{Log. } 3c = 111 \quad = 2 \cdot 0453230$$

$$\text{Log. } a = 7977 \quad = 3 \cdot 9018396$$

$$2) \bar{2} \cdot 1434834$$

$$\bar{1} \cdot 0717417$$

$$\text{Log. sin. } 50^{\circ} . 23' \quad = \bar{1} \cdot 8866756$$

$$\text{Log. sin. } 5^{\circ} . 12' . 49'' \quad = \bar{2} \cdot 9584173$$

$$\text{Cos. } 5^{\circ} . 12' . 49'' \quad = \bar{1} \cdot 9961995$$

2

$$\bar{1} \cdot 9963990$$

$$\text{Ar. comp.} \quad = 0 \cdot 0036010$$

$$\text{Log. } a-2c=7903 \quad = 3 \cdot 8977920$$

$$\text{Log. } 7968 \cdot 8 \quad = 3 \cdot 9013930$$

Ther. $R = \frac{7968.8}{2} = 3984.4 =$ the required radius of curvature. By Example 4th, the radius is 3984.45.

In this Example, a and b represent the whole axes, therefore $2R$ is used instead of R .

EXAMPLE 16.

Given the lengths of two meridional degrees at the equator, and in lat. 45° . N. 68-732 and 69-092 English miles respectively, to find the compression.

Let $\frac{68.732}{69.092} = v$. Then (Cor. 3. Prop. XVIII.) $\frac{OE - OK}{OE} = \frac{(1+v)(1-v)}{2 \sin^2 45^\circ}$.

$$\text{Log. } 68.732 \quad . \quad . \quad . \quad . \quad . = 1.8371590$$

$$\text{Log. } 69.092 \text{ (a} \cdot \text{C)} \quad . \quad . \quad . \quad . \quad . = 2.1605722$$

$$3) \bar{1}.9977312$$

$$\text{Log. } v = .99826 \quad . \quad . \quad . \quad . \quad . = \bar{1}.9992437$$

$$\text{Log. } 1+v = 1.99826 \quad . \quad . \quad . \quad . \quad . = 0.3006520$$

$$\text{Log. } 1-v = 0.00174 \quad . \quad . \quad . \quad . \quad . = \bar{3}.2405492$$

$$\text{Log. } 2(a \cdot c) \quad . \quad . \quad . \quad . \quad . = \bar{1}.6989700$$

$$\text{Log. } \sin^2 45^\circ (a \cdot c) \quad . \quad . \quad . \quad . \quad . = 0.3010300$$

$$\bar{3}.5412012$$

$$\text{Log. } 287.6 \text{ arith. comp.} \quad . \quad . \quad . \quad . \quad . = 2.4587988$$

Therefore the compression is $\frac{1}{287.6}$. By Cor. 2. Prop. XVIII.

The compression is $\frac{1}{287}$.

OF
CENTRIPETAL AND CENTRIFUGAL
FORCES
IN
ELLIPTICAL ORBITS.



CENTRIPETAL FORCES.

DEFINITION 1.

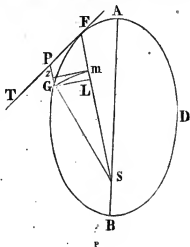
A CENTRIPETAL FORCE is that by which a moving body is continually drawn from its rectilinear motion, and is perpetually solicited towards some center.

DEFINITION II.

A *Centrifugal Force* is the resistance made by a moving body to its being turned out of its rectilinear motion. And because action and re-action are equal and contrary, it follows that in a circle the centripetal and centrifugal forces are equal.

DEFINITION III.

The *centrifugal* force of a body at any point in its orbit, is equal to the *centripetal* force with which the body would describe a circle at the same distance, and with the same velocity, in a direction perpendicular to that distance.



Thus, let $AFBD$ be an elliptic orbit described by a body about the focus S ; let FG be described in an indefinitely little part of time; join SF , SG , and draw the tangent FT , draw GP parallel, and GL perpendicular to SF ; with the center S , and distance SG describe the circular arc Gm , and draw mz parallel to GL . Then will GP represent the centripetal, and $Lm=Gz$, the centrifugal forces at the point F .

DEFINITION IV.

If a body describe an orbit round an immovable center of force, the areas described by lines drawn from the body to the center, are in the same plane, and proportional to the times.

PROPOSITION I. FIG. 1.

If the ellipses AGD , agd , be described about the common focus S , and SQ , Sq be drawn perpendicular to the tangents FP , fp ; vel. at F : vel. at f :: $\frac{\text{area } SFG}{SQ} : \frac{\text{area } Sfg}{Sq}$.

Let FG , fg , be described in indefinitely little equal parts of time; and join SF , SG , Sf , Sg ; then will $SQ \times FG : Sq \times fg :: \text{area } SFG : \text{area } Sfg$; ther. $\frac{\text{area } SFG}{SQ} : \frac{\text{area } Sfg}{Sq} :: FG : fg :: \text{vel. at } F : \text{vel. at } f$.

COR. 1. In the same orbit, $SFG=Sfg$; in that case, vel. at F : vel. at f :: $\frac{1}{SQ} : \frac{1}{Sq}$.

COR. 2. When F , f , coincide with A , a , $SQ=SA$, and $Sq=Sa$; then, vel. at A : vel. at a :: $\frac{\text{area } SAG}{SA} : \frac{\text{area } S ag}{Sa} :: \frac{1}{SA} : \frac{1}{Sa}$ (in the same orbit).

COR. 3. If F , f , coincide with B , we then have vel. at B :

vel. at $b :: \frac{\text{area } S B G}{S B} : \frac{\text{area } S b g}{S b} :: \frac{1}{S B} : \frac{1}{S b}$ (in the same orbit).

Cor. 4. If F, f coincide with N, n , then $SQ = CN$, and $Sq = cn$; we shall then have vel. at $N : \text{vel. at } n :: \frac{\text{area } S N G}{C N} : \frac{\text{area } S n g}{c n} :: \frac{1}{C N} : \frac{1}{c n}$ (in the same orbit). AB, ND, ab, nd , the transverse and conjugate axes of the ellipses AGD, agd ; and G, g , are always supposed to be indefinitely near to F and f .

PROP. II. FIG. 1.

If a body revolve in an ellipse AGD , to find the centripetal force tending to the focus S .

Let S be the focus of the ellipse, AB the greater axes, C the center, and CD half the less axis; let FG, fg , be described in indefinitely equal parts of time; join SF, SG, Sf, Sg ; draw SQ perpendicular to the tangent at F , draw GP parallel to SF , and CI parallel to FP ; let FEH be the circle of curvature at F , and FE the chord passing through the focus.

The centripetal force $PG \propto \frac{FG^2}{FE} \propto \frac{\text{vel.}^2}{FE}$ (1. cir. cur.); but (Cor. 1. Prop. I.) $\text{vel.}^2 \propto \frac{1}{SQ^2} \therefore PG \propto \frac{1}{FE \times SQ^2}$; but (31 Ellip.) $SQ^2 = \frac{SF^2 \times CD^2}{CI^2}$, and (3. cir. cur.) $FE = \frac{2CI^2}{AC}$; ther. $PG \propto \frac{CA}{2CI^2} \times \frac{CI^2}{SF^2 \times CD^2} \propto \frac{1}{SF^2} \times \frac{CA}{2CD^2} \propto \frac{1}{SF^2}$, because CA and CD are given.

Therefore, centripetal force at $F : \text{centrip. force at } f :: \frac{1}{SF^2} : \frac{1}{Sf^2}$.

PROP. III. FIG. 2.

If a body revolve in an ellipse AGD , to find the centripetal force tending to the center C .

Let C be the center of the ellipse, AB the greater axis, and CD half the less axis; let FG, fg , be described in indefinitely little equal parts of time; join CF, CG, Cf, Cg ; draw CQ perpendicular to the tangent at F ; draw GP parallel to CF , and CI parallel to FP ; let FEH be the circle of curvature at F , and FE the chord of curvature passing through the center C .

By Prop. II. $PG \propto \frac{1}{FE \times CQ^2}$, and (Cor. 1. §1. Ellip.) $CQ^2 = \frac{AC^2 \times CD^2}{CI^2}$; and (1. cir. cur.) $FE = \frac{2CI^2}{CF}$; therefore $PG \propto \frac{CF}{2CI^2} \times \frac{CI^2}{CA^2 \times CD^2} \propto CF \times \frac{1}{2CA^2 \times CD^2} \propto CF$, because CA and CD are given; therefore centrip. force at F : centrip. force at f :: CF : Cf .

PROP. IV. FIG. 1.

If a body be projected from a given point F , in a given direction FP , with a given velocity, and at the same time be acted upon by a centripetal force, which varies inversely as the squares of the distances from S , it will describe an ellipse whose focus is S .

Let S be the center of force, F the given point in the curve, and FP a tangent at F , the given direction; Let FG be described in an indefinitely little part of time; draw SF, SG ; draw GP parallel to SF , and SQ perpendicular to FP ; and let L represent the latus-rectum.

If the curve be an ellipse, we have (Prop. IV. V. cir. cur.) $SF^2 : SQ^2 :: \frac{GF^2}{GP} : L$; but (Prop. II.) $GP \propto \frac{1}{SF^2}$; therefore $SF^2 : SQ^2 :: GF^2 \times SF^2 : L = SQ^2 \times GF^2$; but SP and the angle SFQ are given, therefore SQ may be found; and FG (being indefinitely little) will represent the velocity, which is also given; therefore L , the latus-rectum, is given. Hence we have sufficient data to describe the ellipse; therefore the body will revolve in the ellipse with those data; for it cannot describe any other curve with the same data. For a construction see Prop. XLVI. Ellipse.

PROP. V. FIG. 1.

Bodies describing ellipses AGD , agd , about the same common focus S , with forces which vary inversely as the squares of the distances from the focus, will have their principal latera-recta to each other, in the duplicate ratio of the areas described in the same time.

Let FG , fg , be described in indefinitely little equal parts of time, join SF , SG , Sf , Sg ; draw GL , gl , perpendicular, and GP , gp , parallel to SF , Sf , respectively; put L =latus-rectum of AGD , and l =latus-rectum of agd .

Then (aréa SFG)² : (aréa Sfg)² :: $SF^2 \times GL^2$: $Sf^2 \times gl^2$;

But (5. cir. cur.) $GL^2 = GP \times L$, and $gl^2 = gp \times l$;

But (Prop. II.) $GP \propto \frac{1}{SF^2}$, and $gp \propto \frac{1}{Sf^2}$;

Therefore (aréa SFG)² : (aréa Sfg)² :: $L : l$.

Cor. If one of the orbits (agd) be a circle, then l =diameter of that circle. In that case,

Area in the ellipse : aréa in the circle :: $\sqrt{\text{Latus-rectum}}$: $\sqrt{\text{Diam.}}$

PROP. VI. FIG. 1.

The *squares* of the periodic times in all ellipses described about the same common focus, are as the *cubes* of their transverse axes.

Let AB , ND , a , b , nd , be the transverse and conjugate axes of the two ellipses AGD , agd , described about the common focus S ; let FG , fg , be described in indefinitely little equal parts of time; join SF , SG , Sf , Sg ; let P represent the periodic time in the orbit $ANBD$, and p the periodic time in the orbit $anbd$; put L and l , for their respective latera-recta.

Conceive the areas of these ellipses to be made up of the indefinitely little triangles SFG , Sfg ; and as these areas are proportional to the times of describing, it will be

$P \times SFG : p \times Sfg :: ANBD : anbd$;

But (Prop. V.), $(SFG)^2 : (Sfg)^2 :: L : l$,

Ther. $P^2 \times L : p^2 \times l :: AB^2 \times DN^2 : ab^2 :: dn^2$,

That is, $P^2 : p^2 :: \frac{AB^2 \times DN^2}{L} : \frac{ab^2 \times dn^2}{l} :: AB^2 : ab^2$.

COR. 1. The periodic times are as the rectangles of their axes directly, and subduplicate ratio of their latera-recta inversely.

For, $P : p :: \frac{AB \times DN}{\sqrt{L}} : \frac{ab \times dn}{\sqrt{l}}$.

COR. 2. If the ellipses become circles, the transverse and conjugate diameters, and the latera-recta become equal to each other; then the squares of the periodic times will be as the cubes of the diameters.

COR. 3. If one of the ellipses (abn) become a circle, the diameters of which are equal to the transverse diameter AB ; the periodic times in the ellipse and circle will be equal.

PROP. VII. FIG. 1.

If in bodies describing ellipses AGD , agd , about the same common focus S , with forces which vary inversely as the squares of the distances from the focus, SQ , Sq ; are perpendiculars to the tangents at F , f , and L , l , are put for the principal latera-recta, then

Vel. at F : vel. at $f :: \frac{\sqrt{L}}{SQ} : \frac{\sqrt{l}}{Sq}$.

Let FG , fg , be described in indefinitely little equal parts of time; join SF , SG , Sf , Sg ; then FG , fg , will represent the velocities at the points F , f .

And $SFG : Sfg :: FG \times SQ : fg \times Sq :: \sqrt{L} : \sqrt{l}$ (Prop. V.);

Ther. $\frac{\sqrt{L}}{SQ} : \frac{\sqrt{l}}{Sq} :: FG : fg :: \text{vel. at } F : \text{vel. at } f$.

COR. 1. The latera-recta are to each other as vel.² $\times$ perpend.². For, $FG^2 \times FQ^2 : fg^2 \times fq^2 :: L : l :: (\text{vel.}^2 \text{ at } F) \times SQ^2 : (\text{vel.}^2 \text{ at } f) \times Sq^2$.

COR. 2. If the ellipses become circles, then $L = 2AC$, $SQ =$

AC, $l=2ac$, $Sq=ac$; and the analogy in the Proposition becomes,

Vel. at F : vel. at f :: $\frac{\sqrt{2AC}}{AC} : \frac{\sqrt{2ac}}{ac} :: \frac{1}{\sqrt{AC}} : \frac{1}{\sqrt{ac}}$;
AB, a b, being the transverse axes.

Cor. 3. When F coincides with A, then $SQ=SA$; and if the ellipse a n b d becomes a circle whose radius= $SA=Sq$, and therefore $l=2SA$; we have $FG : fg :: \frac{\sqrt{L}}{SA} : \frac{\sqrt{2SA}}{SA} :: \sqrt{L} : \sqrt{2SA}$; that is, vel. at F : vel. at f :: $\sqrt{L} : \sqrt{2SA}$.

Cor. 4. In the same manner, when F coincides with B, and the ellipse a n b d becomes a circle, we have vel. at F : vel. at f :: $\sqrt{L} : \sqrt{2SB}$.

Cor. 5. When F coincides with N, then $SF=SN=AC$, and $SQ=CN$. And if the ellipse a n b d, becomes a circle whose radius= $SN=AC$, therefore $l=2AC$, and $Sq=AC$, the general proportion becomes $FG : fg :: \frac{\sqrt{L}}{CN} : \frac{\sqrt{2AC}}{AC}$; ther. $FG^2 : fg^2 :: \frac{L}{CN^2} : \frac{2AC}{AC^2} :: \frac{2}{AC} : \frac{2}{AC} \therefore FG=fg$.

Therefore the velocities of bodies revolving in ellipses at the mean distances, are equal to those in circles at the same distances.

Cor. 6. If the ellipse a n b d becomes a circle, whose radius= $SF=Sf=SQ$; and ther. $l=2SF$; we then have $FG^2 : fg^2 :: \frac{L}{SQ^2} : \frac{2SF}{SF^2} = \frac{2}{SF}$; ther. $FG^2 : fg^2 :: SF \times L : 2 \times SQ^2 :: SF \times \frac{1}{2}L : SQ^2$; or, $FG : fg :: \sqrt{SF \times \frac{1}{2}L} : SQ ::$ vel. in ellip. : vel. in circle when the distance SF =radius of the circle.

PROP. VIII. FIG. 1.

Let the ellipses AGD, a g d, be described about the common focus S, with forces which vary inversely as the squares of the distances from the focus; then angular vel. at F : angular vel. at f ::

$$f :: \frac{SFG}{SF^2} : \frac{Sfg}{Sf^2}.$$

Let FG, fg , be described in indefinitely little equal parts of time; join SF, SG, Sf, Sg ; and we then have $SF \times SG \times \sin. FSG : Sf \times Sg \times \sin. fSg :: SFG : Sfg$;

$$\text{Ther. } \sin. FSG : \sin. fSg :: \frac{SFG}{SF \times SG} : \frac{Sfg}{Sf \times Sg};$$

That is, ang. vel. at F : ang. vel. at f :: $\frac{SFG}{SF^2} : \frac{Sfg}{Sf^2} :: \frac{1}{SF^2} : \frac{1}{Sf^2}$
in the same orbit; for then SFG, Sfg would be equal.

$$\text{Cor. 1. Ang. vel. at } F : \text{ang. vel. at } f :: \frac{\sqrt{L}}{SF^2} : \frac{\sqrt{l}}{Sf^2} (\text{Prop. V.})$$

Cor. 2. The angular velocity in an ellipse at a mean distance, is to that in a circle at the same distance, as the conjugate axis to the transverse axis.

When F coincides with N , then $SF=SN=AC$, and $SQ=CN$; and if the ellipse anb becomes a circle whose radius $=SN=AC=Sf$, then $l=2AC$.

Let ϕ =angular velocity in the ellipse, and θ =angular velocity in the circle; then the proportion in cor. 1. will become,

$$\phi : \theta :: \frac{\sqrt{L}}{AC^2} : \frac{\sqrt{2AC}}{AC^2} :: \sqrt{L} : \sqrt{2AC};$$

$$\text{Ther. } \phi^2 : \theta^2 :: L : 2AC :: \frac{2CN^2}{AC} : 2AC :: 2CN^2 : 2AC^2;$$

That is, $\phi : \theta :: CN : AC :: \text{ang. vel. in ellip.} : \text{ang. vel. in circle.}$

$$\begin{aligned} \text{Cor. 3. Since } \phi : \theta :: \frac{\sqrt{L}}{SF^2} : \frac{\sqrt{2AC}}{AC^2}; \text{ then if } \phi = \theta, \frac{\sqrt{L}}{SF^2} \\ = \frac{\sqrt{2AC}}{AC^2} \therefore SF^2 = \frac{AC^2 \sqrt{L}}{\sqrt{2AC}} = \frac{AC^2}{\sqrt{AC} \times \sqrt{2}} \times \frac{CD \times \sqrt{2}}{\sqrt{AC}} = \\ AC \times CD; \text{ ther. } SF = \sqrt{AC \times CD}. \end{aligned}$$

Hence the distance in the ellipse may be found, at which the angular velocity is equal to that in the circle at the same distance.

PROP. IX. FIG. 1.

Let AGD be an ellipse, described by a body acted upon by a centripetal force tending to the focus S .

The centrifugal force at F : centrifugal force at f :: $\frac{1}{SF^3} : \frac{1}{Sf^3}$.

Suppose the body in the same indefinitely little part of time to describe the arcs FG, fg ; with the center S , and distances SG, Sg , describe the circular arcs Gm, gv ; draw GL perpendicular to SF , and gl perpendicular to Sf ; then Lm will represent the centrifugal force at F , and lv the centrifugal force at f .

Because FG, fg , are indefinitely little; $SF^2 \times GL^2 = Sf^2 \times gl^2$; and $Lm : lv :: \frac{GL^2}{SL} : \frac{gl^2}{Sf} :: \frac{GL^2}{SF} : \frac{gl^2}{Sf}$, ultimately; but $\frac{GL^2}{SF} = \frac{SF^2 \times gl^2}{Sf^2}$, and $\frac{gl^2}{Sf} = \frac{SF^2 \times GL^2}{Sf^2}$; therefore $Lm : lv :: \frac{SF^2 \times gl^2}{Sf^2} : \frac{SF^2 \times GL^2}{Sf^2} :: \frac{1}{SF^3} : \frac{1}{Sf^3}$.

Ther. centrif. force at F : centrif. force at f :: $\frac{1}{SF^3} : \frac{1}{Sf^3}$.

PROP. X. FIG. I.

Let AGD be an ellipse described by a body acted upon by a centripetal force tending to the focus S ; then centripetal force at F : centrifugal force at F :: $2SF^2 : SQ^2 \times FE$.

Let FH be the diameter of the circle of curvature at F ; FE , the chord of curvature passing through the focus S ; draw SQ perpendicular to the tangent at F , and GL perpendicular to SF ; draw Gz parallel to FP ; with the center S , and distance SG , describe the circular arc Gm , and join HE .

In the similar triangles GLz, SFQ , we have $Gz^2 : GL^2 :: SF^2 : SQ^2$. But centrip. force at F : centrif. at F :: $Fz : Lm$;

But (ultimately) $Fz = \frac{Gz^2}{FE}$, and $Lm = \frac{GL^2}{2SG} = \frac{GL^2}{2SF}$; therefore

$Fz : Lm :: \frac{SF^2}{FE} : \frac{SQ^2}{2SF} :: 2SF^2 : SQ^2 \times FE :: \text{Centrip. force at } F : \text{centrif. force at } F$.

Cor. 1. By 31 Ellip. $SQ^2 = \frac{SF^2 \times CD^2}{CI^2}$, and (3 cir. cur.)

$FE = \frac{2CI^2}{AC}$; ther. $SQ^2 \times FE = \frac{2SF^2 \times CD^2}{AC}$; hence we have
centrip. force at F : centrif. force at F :: $2SF^2 : \frac{2SF^2 \times CD^2}{AC} ::$
 $SF : \frac{CD^2}{AC}$; $SF : \frac{1}{2}$ latus-rectum.

COROLLARY 2.

If the centripetal force $GP = Fz$, at any point F, be put = M, and the centrifugal force at the same point, be put = N, the principal latus-rectum being $tT = XY \dots\dots\dots = L$,

We shall then have the following proportions:

$$M : N :: \left\{ \begin{array}{l} SF : \frac{CD^2}{AC} :: SF : \frac{1}{2}L \\ *SA : \frac{CD^2}{AC} :: CB : BS \\ \dagger SB : \frac{CD^2}{AC} :: CB : AS \\ SN : \frac{CD^2}{AC} :: CB^2 : CD^2 \\ \left\{ \begin{array}{l} St : \frac{CD^2}{AC} :: \frac{1}{2}L : \frac{1}{2}L \\ \text{Therefore } \dots M = N \end{array} \right\} \\ \dagger SX : \frac{CD^2}{AC} :: AB - \frac{1}{2}L : \frac{1}{2}L \end{array} \right\} \begin{array}{l} \text{-- } \left\{ \begin{array}{l} \text{Any point in the} \\ \text{Ellipſe,} \end{array} \right. \\ \text{-- the point A,} \\ \text{-- the point B,} \\ \text{-- D or N,} \\ \text{-- T or t,} \\ \text{-- X or Y.} \end{array} \begin{array}{l} \text{When F is at} \end{array}$$

SCHOLIUM.

Hence it appears that if a body revolve in an elliptic orbit AGD, about the focus S, and is acted upon by a centripetal force, which varies inversely as the squares of the distances from the focus, during the time the body is describing the space

$$\begin{aligned} * SA : \frac{CD^2}{AC} &:: AC + CS : \frac{(AC + CS)(AC - CS)}{AC} :: AC : AC - CS \\ CS &:: CB : BS. \\ \dagger SB : \frac{CD^2}{AC} &:: AC - CS : \frac{(AC + CS)(AC - CS)}{AC} :: AC : AC + CS \\ CS &:: CB : AS. \\ \dagger SX + XM &= AC \therefore SX = AC - MX = AB - \frac{1}{2}L. \end{aligned}$$

T D t, the centripetal force will exceed the centrifugal force: and while it is describing the space t B T, the centrifugal force will exceed the centripetal force: and at the points t and T, the both forces will be equal.

PROP. XI. FIG. 1.

If a body describe an ellipse A G D, about the focus S, with forces which vary inversely as the squares of the distances from the focus; the velocity in the ellipse is to that of a body revolving in a circle at the same distance from the center, in a less ratio, than $\sqrt{2}$ to 1.

Let A B, D N, be the transverse and conjugate diameters; S, M, the foci, and C the center; let F G be described in an indefinitely little part of time; join S F, S G, S N, M F; draw G P parallel to S F, and C I parallel to the tangent F P; let F E H be the circle of curvature at F, and F E the chord passing through the focus S.

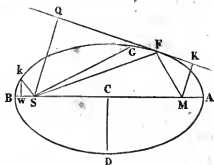
Then (1. cir. cur.) vel. $\propto \sqrt{P G \times F E} \propto \sqrt{P G \times \frac{2 C I^2}{A C}}$, (3. cir. cur.); in a circle C I = C A; in that case, vel. $\propto \sqrt{P G \times 2 A C}$; ther. vel. in the ellipse at F: vel. in a circle at the same distance :: $\sqrt{P G \times \frac{2 C I^2}{A C}} : \sqrt{P G \times 2 A C} :: \sqrt{\frac{2 C P^2}{A C}} : \sqrt{2 S F}$ (in the circle A C = S F) :: $\sqrt{\frac{2 S F \times F M}{A C}} : \sqrt{2 S F} :: \sqrt{F M} : \sqrt{A C} :: \sqrt{2 A C - S F} : \sqrt{A C}$; by 26 Ellip. $S F \times M F = C P^2$, and 10 Ellip. $F M = 2 A C - S F$. Therefore the velocity in the Ellipse at F, is to the velocity in a circle at the same distance, as $\sqrt{2 A C - S F}$ to $\sqrt{A C}$, which is always less than $\sqrt{2}$ to 1.

Cor. When $S F = S N = A C$ (6 Ellip.), then the velocity in the ellipse in F is equal to the velocity in the circle.

PROP. XII.

Supposing a body acted upon by a centripetal force tending to the focus S, describe the ellipse B F A D, to be projected from

a given point F , in a given direction FQ with a given velocity, to find the axes of the ellipse and the periodic time.



Let AB be the greater axis, CD half the lesser, and S, M , the foci; suppose FG to be an indefinitely small part of the curve described in the particle of time t , and f a space, a body will descend at F in the time t by the centripetal force; join SG , and make the area SBk equal to SFG ; demit the perpendiculars SQ, MK, kw , and put s for the nat. sin. (rad. 1.) of the angle SFQ , or MFK ; we shall then have

$$SQ^2 : SB^2 :: Bk^2 : FG^2 \text{ from the equal triangles,}$$

$$SB^2 : SF^2 :: f : Bw \text{ proposition 2.}$$

$$AB : 4CD^2 :: Bw : Bk^2 \text{ proposition 5 cir. cur.}$$

$$4CD^2 : 4SQ^2 :: MK : 1 \text{ proposition 26 ellipse.}$$

$$\text{From whence } AB.SQ : 4SF^2 :: f.MK : FG^2.$$

$$\text{Therefore } AB = \frac{4f.MK.SF^2}{SQ.FG^2} = \frac{4f.SF(AB-SF)}{FG^2} =$$

$$\frac{4f.SF^2}{4f.SF-FG^2}, \text{ and } CD^2 = s^2.SF(AB-SF) = \frac{s^2.SF^2.FG^2}{4f.SF-FG^2}$$

$$\therefore CD = \frac{s.SF.FG}{(4f.SF-FG^2)^{\frac{1}{2}}}, \text{ and } FM = AB-SF =$$

$$\frac{SF.FG^2}{4f.SF-FG^2}.$$

Now since FM and the angle MFK are given, the focus M is given; therefore the position of the transverse axis AB is given.

To find the Periodic Time.

By putting p for the circumference of a circle whose diameter is unity, the area of the ellipse will be $AB \cdot 2CD \cdot \frac{p}{4} = \frac{2psf \cdot FG \cdot SF^2}{(4f \cdot SF - FG^2)^{\frac{3}{2}}}$. Then, def. 4. $\frac{s \cdot SF \cdot FG}{2} : t :: \frac{2psf \cdot FG \cdot SF^2}{(4f \cdot SF - FG^2)^{\frac{3}{2}}} : \frac{4pft \cdot SF^2}{(4f \cdot SF - FG^2)^{\frac{3}{2}}}$ time of one revolution.

Cor. 1. $\frac{4CD^2}{AB} = \frac{s^2 \cdot FG^2}{f} = \text{latus-rectum of the transverse axis AB.}$

Cor. 2. The transverse axis and periodic time will remain the same, whatever be the angle of direction SPQ ; for their values are not affected with s .



THE FIRST
OF
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PROP. I. FIG. 1.

LET ABC be any curve whose axis is AD ; and let EFG be a curve line, so related to ABC , that if from any point H in AD there be drawn HB perpendicular to AD , meeting the curves ABC , EFG , in B and F , and if from B there be drawn the tangent Bf , meeting AD in f , so that $fH \times HF : HB^2 :: p : q$, a given ratio; and if AE be drawn perpendicular to AD ; then will $fH \times HF = 2 \times \text{area } AEFH$.

Let AH be divided into indefinitely little parts, in the points K, L, M , &c.; draw KN, LO, MP , &c. parallel to HB , meeting the curves in N, O, P, Q, R, S , &c.; draw BT parallel to AD ; and let $HB \times BT = fH \times HF$, and join HT ; draw NV, OX, PY , &c. parallel to AD ; and let NZ be a tangent to the curve at N ; let NV meet BH in a , and OX meet BH, NK , in b, c .

Because $HB \times BT = fH \times HF$, $BT : HF :: fH : HB :: Na (KH) : Ba$, (the triangles fHB, NaB , being considered as similar); ther. $aB \times BT = KH \times HF$. Again, because $ZK \times KQ : KN^2 (Ha^2) :: p : q :: fH \times HF : HB^2$, and $Ha^2 : Ha \times aV :: HB^2 : HB \times BT$; ther. $ZK \times KQ : Ha \times aV :: fH \times HF : HB \times BT$; therefore $ZK \times KQ = Ha \times aV \therefore Va : KQ :: ZK : Ha (KN) :: oc (LK) : CN (ab)$; ther. $Va \times ab = KQ \times LK$.

Again let PY meet BH in d , and in the same way it is shown that $db \times bX = ML \times LR$, and so on; ther. the sum of the rectangles aBT, baV, dbX , &c. is equal to the sum of the

rectangles KHF , LKQ , MLR , &c. But the former sum may be considered equal to the triangle HBT , and the latter sum to the figure $AEFH$: but $fH \times HF = HB \times BT = \text{double the triangle } HBT$; ther. $fH \times HF = 2 \times \text{area } AEFH$. Q. E. D.

From the general proportion we have $HF : KQ :: \frac{HB^2}{fH} : \frac{KN^2}{ZK}$; that is, HF , KQ , &c. are as the squares of the ordinates directly, and subtangents inversely.

PROP. II. FIG. 2.

Let there be a curve ABC , whose axis is AD ; and let EFG be a curve, whose asymptote is AH , perpendicular to AD ; let the curves be so related to each other, that if from any points B , C , in ABC , there be drawn BK , CD , perpendicular to AD , meeting the curve EFG in F , G ; and let BL , CM , be tangents to ABC at the points B and C ; and if $MD \times DG : LK \times KF :: CD : BK$; the figure $HADGE = MD \times DG$.

Draw FN parallel to BL ; let CD be divided into indefinitely little parts in O , P , Q , R , S , &c.; draw OT , PV , QX , RY , SZ , &c. parallel to AD ; and draw Ta , Vb , Xc , Yd , Zc , &c. parallel to CD , meeting the curve EFG in f , g , h , k , l , &c.; draw the tangents Tm , Vo ; and let VP meet Ta in p .

Because FN is parallel to BL , $BK : KN :: FK : KN$; ther. $BK \times KN = LK \times KF$; but (by hypoth.) $MD \times DG : LK \times KF :: CD : BK :: CD \times KN : BK \times KN \therefore MD \times DG = CD \times KN$; ther. $DG : KN :: CD : MD :: CO : OT (Da) \therefore GD \times Da = CO \times KN$.

Again, because $ma \times af : LK \times KF :: aT : BK :: aT \times KN : BK \times KN \therefore ma \times af = aT \times KN$; ther. $af : KN :: Ta : am :: Tp : pV (ab) \therefore af \times ab = KN \times Tp = KN \times OP$. In the same way it may be shewn that $gb \times bc = PQ \times KN$, and so on; therefore $GDa + fab + gbc + \&c. = CO \times KN + OP \times KN + PQ \times KN + \&c. = (CO + OP + PQ + \&c.) \times KN = CD \times KN = MD \times DG$; but the sum of the rectangles GDa , fab , gbc , &c. may be considered equal to the figure $HADGE$, as

well as $CO + OP + PQ + \&c. = CD$; ther. $HADGE = MD \times DG$. Q.E.D.

PROP. III. FIG. 3.

Let a body descend in the line AB from A , supposing any centripetal force whatever: let CDE be a curve, such, that if from any two points F, G , FD, GE , be drawn perpendicular to AB , so that centripetal force at F : centripetal force at $G :: FD : GE$, and AC be drawn perpendicular to AB ; then will velocity at F : velocity at $G :: \sqrt{ACDF} : \sqrt{ACEG}$.

Let AHK be a curve, such, that if from any points F, G , there be drawn FH, GK , perpendicular to AB , so that $FH : GK :: \text{vel. at } F : \text{vel. at } G$, and HL, KM , be tangents to the curve in H , and K ; let FN, GO , be spaces passed over, in an indefinitely little part of time; draw NP, OQ , perpendicular to AB ; and HR, KS , parallel to AB ; and let $KG \times GT = FH \times GE$, or $GK : FH :: GE : GT$.

Because $FH : NP :: \text{vel. at } F : \text{vel. at } N$,

And - - - $GK : OQ :: \text{vel. at } G : \text{vel. at } O$,

Also - - - $PR : QS :: \text{incr. of vel. at } F : \text{incr. vel. at } G$,

The velocities being as the forces and times, and the times being equal, the velocities are therefore as the forces: therefore $PR : QS :: \text{centrip. force at } F : \text{centrip. force at } G :: FD : GE :: FD \times FH : GE \times FH = KG \times GT$; and because the spaces FN, GO , are passed over in the same time, and the spaces being as the velocities and times;

Ther. $\text{vel. } F : \text{vel. at } G :: FN : GO :: HR : KS$,

But $HR : RP :: LF : FH :: LF \times FD : FH \times FD$;

And $RP : QS :: FD \times FH : KG \times GT$;

Ther. $HR : QS :: LF \times FD : KG \times GT$;

But $QS : SK :: KG : GM :: KG \times GT : GM \times GT$;

Ther. $HR : SK :: LF \times FD : GM \times GT$;

But $\text{vel. at } F : \text{vel. at } G :: HR : KS :: FH : GK$ (hypoth.)

Ther. $FH : GK :: LF \times FD : GM \times GT :: FH^2 : FH \times GK :: FH \times GK : GK^2$;

But (hypoth.) $FH : GK :: GT : GE :: GT \times MG : GE \times MG :: FH \times GK : GK^2$;

Ther. $LF \times FD : MG \times GE :: FH^2 : GK^2$; ther. (Prop. 1), $LF \times FD = 2 \times \text{area } ACDF$, and $MG \times GE = 2 \times \text{area } ACGE$.

Ther. $LF \times FD : MG \times GE :: ACDF : ACGE :: FH^2 : GK^2$;

Ther. $FH : GK :: \sqrt{ACDF} : \sqrt{ACGE} :: \text{velocity at } F : \text{velocity at } G$. Q. E. D.

PROP. IV. FIG. 4.

Let a body descend from A, in the line AB with any centripetal force, and let CDE be a curve, such, that if from any two points F, G, FD, GE, be drawn perpendicular to AB, and that $GE : FD :: \text{vel. at } F : \text{vel. at } G$; and let AH, perpendicular to AB, be the asymptote of the curve CDE; then will the

Time of descent through AF : time of descent through AG :: HAFDC : HAGEC.

Let AKL be a curve, such, that drawing FK, GL, perpendicular to AB, so that

$FK : GL :: \text{time of descent through AF} : \text{time of descent through AG}$, draw the tangents KM, LN; and let FO, GP, be the spaces passed over by the body in an indefinitely little part of time, when at F and G; draw OQ, PR, perpendicular, and KS, LT, parallel to AB.

Because $PR : GL :: \text{time descent through AP} : \text{time descent through AG}$,

And $OQ : FK :: \text{time descent through AO} : \text{time descent through AF}$,

Then $RT : QS :: \text{time descent through GP} : \text{time descent through FO}$,

But, the time of descent through GP = the time of descent through FO,

Therefore $RT = QS$. Because the spaces GP, FO, are passed over in equal times.

The vel. at G : vel. at F :: GP : FO :: LT : KS,

Since, $MF \times FD : MF \times EG :: FD : EG :: LT : KS$,
 And $MF \times EG : FK \times EG :: MF : FK :: KS : SQ$,
 Ther. $MF \times FD : FK \times EG :: LT : SQ$ (RT) $:: NG : GL$
 $:: NG \times GE : GL \times GE$.
 And $MF \times FD : NG \times GE :: FK \times GE : GL \times GE :: FK$
 $: GL$.

Therefore (Prop. II.) $HAFDC = MF \times FD$, and $HAGEC$
 $= NG \times GE$;

Hence $FK : GL :: HAFDC : HAGEC$;

Ther. time of descent through AF : time of descent through
 $AG :: HAFDC : HAGEC$. Q.E.D.

PROP. V. FIG. 5.

Suppose a body to descend from A , in the line AB , and AC
 DE to be a curve so related to AB , that if from any two points
 F, G , there be drawn FC, DG , perpendicular to AB , and that
 the vel. at F : vel. at $G :: \sqrt{FC} : \sqrt{GD}$, and the tangents CH ,
 DK , be drawn; then will the centripetal force at F : centripetal
 force at $G :: \frac{FC}{FH} : \frac{GD}{GK}$.

Let LMN be a curve so related to AB , that CF, DG , being
 produced to M and N , the centripetal force at F : centripetal
 force at $G :: FM : GN$; take FO , indefinitely little, draw OP
 parallel to FC ; take GQ equal to FO , and draw QR parallel
 to GD ; draw CS, DT , parallel to AB ; produce PO and RQ ,
 to meet the curve LMN , in V and X ; and draw AL perpen-
 dicular to AB .

Because vel. at F : vel. at $G :: \sqrt{FC} : \sqrt{GD} :: \sqrt{LAFM} :$
 $\sqrt{LAGN}$ (Prop. III.)

Ther. $LAFM : LAGN :: FC : GD$; which proportion
 shows the relation of the curves ACD, LMN , to each other.

Ther. $LAOV : LAFM :: OP : FC$,

And, $MF \times FO : LAFM :: OP - FC : FC :: SP : FC$,

But, $LAFM : LAGN :: FC : GD$,

Ther. $MF \times FO : LAGN :: SP : GD$,

Also, $LAGN : LAQX :: GD : QR$,

Ther. $LAGN : NG \times GQ :: GD : QR - GD = RT$,

And, $MF \times FO : NG \times GQ :: SP : RT$, but $FO = GQ$
(hypoth.)

Ther. $FM : GN :: MF \times FO : NG \times GQ :: SP : RT$,

Because FO and GQ , are indefinitely little, the triangles HFC , CSP , may be considered as similar, as well as the triangles KGD and DTR .

Ther. $HF : FC :: CS (FO) : SP \therefore PS \times HF = CF \times FO$,

In the same way it may be shewn, that $RT \times GK = DG \times GQ$,

Ther. $PS \times HF : RT \times GK :: CF \times FO : DG \times GQ :: FC : DG :: CF \times GK : DG \times GK$,

Hence $PS \times HF : CF \times GK :: RT \times GK : DG \times GK :: RT : DG :: RT \times HF : DG \times HF$,

Ther. $PS \times HF : RT \times HF :: CF \times GK : DG \times HF :: PS : RT :: FM : GN$,

Hence, $FM : GN :: CF \times GK : DG \times HF$,

But hypoth. centrip. force at F : centrip. force at $G :: FM : GN$,

Ther. centrip. force at F : centrip. force at $G :: FC \times GK :$

$GD \times FH :: \frac{FC}{FH} : \frac{GD}{GK}$. Q. E. D.

PROP. VI. FIG. 6.

If a body acted upon by a centripetal force, tending to a fixed center, describe a curve line, the angular velocity of the body round the fixed center will be reciprocally as the square of the distance of the body from the center.

Let ABC be any curve described by a body that is acted upon by a centripetal force, tending to the center S ; draw SA , SB , to any two points A , B , in the curve; the angular vel. of SA : angular vel. of $SB :: SB^2 : SA^2 :: \frac{1}{SA^2} : \frac{1}{SB^2}$.

Let AD , BE , be described in indefinitely little parts of time; join SD , SE : with the center S , and radii SD , SE , describe the arcs FH , EK , meeting SA , SB , SE , in F , G , H , K .

Because AD , BE , are described in equal times, the triangles ASD , BSE , will be equal.

Ther. $\sin. ASD : \sin. BSE :: SB \times SE : SA \times SD$,

That is, $DF : GH :: SB^2 : SA^2 :: \frac{1}{SA^2} : \frac{1}{SB^2}$,

AD , BE , being indefinitely small. Q. E. D.

PROP. VII. FIG. 7.

Let SA , SB , be two right lines intersecting each other in the point S ; and AC , BD , perpendicular thereto; and let AE , BF , be indefinitely little parts described by bodies moving therein in an indefinitely little part of time; and let $BF^2 : AE^2 :: SB : SG$,

Then, centrifugal force at B : centrifugal force at $A :: SA : SG$;

That is, $FL : EH :: SA : SG$,

Join SE , SF ; with the center S , and radii SA , SB , describe circles meeting SE in H and K , and SF in L and M . Because $BF^2 = FM \times FL$, and $AE^2 = EK \times EH$, $BF^2 : AE^2 :: FM \times FL : EK \times EH$.

But BF , AE , being indefinitely small, we may consider $ML = MF$, and $KE = KH$,

Ther. $BF^2 : AE^2 :: LM \times FL : KH \times EH :: SL \times FL : SH \times EH$;

But, $BF^2 : AE^2 :: SB(SL) : SG :: SL \times LF : SG \times LF$,

Ther. $SL \times FL : SH \times EH :: SL \times LF : SG \times LF$,

Hence $SH \times EH = SG \times LF \therefore FL : EH :: SA : SG$.

But FL = centrifugal force at B ,

And EH = centrifugal force at A ,

Ther. centrifugal force at B : centrifugal force at $A :: SA : SG$. Q. E. D.

PROP. VIII. FIG. 8.

Let ABC be any curve, described by a body that is acted upon by a centripetal force, tending to the center S : the centri-

fugal force at B : centrifugal force at A :: $SA^3 : SB^3 :: \frac{1}{SB^3} : \frac{1}{SA^3}$

Suppose a body in the same indefinitely little part of time to describe the arcs AD, BE; draw DK, EL, perpendicular to SA, SB; complete the parallelograms AKFD, BLEG, and let $BG^3 : FA^3 :: SB : SH$; join SD, SE, SF, SG. Because the arcs AD, BE, are indefinitely little, they may be considered as straight lines; the force acting in the direction AD, may be resolved into the forces AF, AK; likewise the force acting in the direction BE, may be resolved into the forces BG, BL. Because AD, BE, are described in equal times, the triangles SDA, SFA; SBE, SBG, will be equal to each other.

Ther. $SA^3 : SB^3 :: BG^3 : AF^3 :: SB : SH \therefore SA^3 \times SH = SB^3$.

Ther. $SA^3 : SB^3 :: SA^3 : SA^3 \times SH :: SA : SH$.

But (Prop. VII.) centrifugal force at B :: centrifugal force at A :: SA : SH.

Ther. centrifugal force at B : centrifugal force at A :: $SA^3 : SB^3 :: \frac{1}{SB^3} : \frac{1}{SA^3}$. Q. E. D.

PROP. IX. FIG. 9.

Supposing a body acted upon by a centripetal force tending to the center S, to be projected at the point A, in the direction AB, perpendicular to SA; and suppose in an indefinitely little part of time, the body would describe AC by the projectile force alone; let AD be the space that would be described in the same time by the centripetal force tending to the center S; then,

Centrifugal force at A : centripetal force at A :: $AC^2 : 2SA \times AD$.

Join SC, and with the center S, and distance SA, describe a circle meeting SC in E and F.

Because $CE : AD :: CE \times FC : AD \times FC :: AC^2 : AD \times FC$, and CE being infinitely little, we may consider $FC = FE$; then $AD \times FC = AD \times FE = 2SA \times AD$.

Ther. $CE : AD :: AC^2 : 2SA \times AD$.

And, centrifugal force at A : centripetal force at A :: $AC^2 : 2SA \times AD$. Q. E. D.

PROP. X. FIG. 10.

Supposing a body, in an indefinitely little part of time, to describe the part AD with an uniform velocity, and a body acted upon by a centripetal force tending to the center S, to describe the part AE, in the same time : then

Vel. at E : vel. in AD :: 2 AE : AD.

Because the time in which AE is described is indefinitely little, the centripetal force may be considered as acting uniformly during such little part of time, therefore the body, with the velocity acquired at E, acting uniformly, would describe twice AE in the same time that AE was described, that is, in the same time that AD was described with an uniform velocity ; therefore, vel. at E : vel. in AD :: 2 AE : AD. Q. E. D.

PROP. XI. FIG. 11.

Supposing a body acted upon by a centripetal force tending to the center S, to descend in the straight line AS from the point A ; let there be a curve CDE, such, that if from any two points A, B, there be drawn AC, BD perpendicular to AS, so that the centripetal force at A : centripetal force at B :: AC : BD ; also let the body at the point B be projected in the direction BF, perpendicular to SB, with the velocity that would be acquired in falling from A to B.

The centrifugal force at B, arising from the projectile force }
in the direction BF - - - - - }

Centripetal force at B, tending to the center S - - - - :
2 × space CABD : SB × BD.

Let the body, in an indefinitely little part of time, descend from B to H by the centripetal force ; and in an equal time, let the body, by the projectile force in the direction BF, describe BG ; draw HK parallel to BD, and let DB × BL = CABD.

Because (Prop. III.) vel. at B, by falling from A to B, :
vel. at H, by falling from B to H, ::

$$\sqrt{CABD} : \sqrt{DBHK}.$$

and the space $CABD = DB \times BL$, and $DB \times BH = DBHK$, because BH is indefinitely little;

Ther. vel. at B : vel. at H :: $\sqrt{DB \times BL} : \sqrt{DB \times BH} : \sqrt{LB} : \sqrt{BH}$.

But the vel. at B , by falling from A to B , is equal to the velocity in BF ; ther. vel. in BF : vel. at H :: $\sqrt{LB} : \sqrt{BH}$;

But (Prop. X.) vel. in BF : vel. at H :: $BG : 2BH$; ther. $BG : 2BH :: \sqrt{LB} : \sqrt{BH} \therefore BG^2 : 4 \times BH^2 :: LB : BH :: 4BH \times LB : 4BH^2 \therefore BG^2 = 4LB \times BH$; but (Prop. IX.) centrifugal force at B : centripetal force at B :: $BG^2 : 2SB \times BH :: 4LB \times BH : 2SB \times BH :: 2LB : SB :: 2LB \times BD : SB \times BD :: 2 \times CABD : SB \times BD$. Q. E. D.

COROLLARY.

In SB take any point a , and draw ac parallel to BD ; let the body at the point B be projected in the direction BF , perpendicular to SB , with a velocity that would be acquired in falling from B to a ;

The centrifugal force at B arising from the projectile force }
in direction BF - - - - - }
Centripetal force at B , tending to the center S - - - - - ::
 $2 \times ca \times BD : SB \times BD$.

This may be demonstrated in the same way as the proposition. Or it may be shewn that the centrifugal force at a : centripetal force at a :: $2 \times ca \times BD : Sa \times ac$.

PROP. XII. FIG. 12.

Let a body acted upon by a centripetal force tending to the center S , describe the curve ABC ; and let AD , BE , be tangents to the curve at any points A , B , in the curve; let SD , SE , be perpendicular to AD , BE .

The vel. at A : vel. at B :: $SE : SD$.

Join SA , SB , and let AF , BG , be parts of the curb described in indefinitely little equal parts of time; join SF , SG , because AF , BG , are described in equal times, the triangles ASF , BSG

will be equal; therefore $AF : BG :: SE : SD$; but $AF : BG :: \text{vel. at A} : \text{vel. at B}$. Therefore the $\text{vel. at A} : \text{vel. at B} :: SE : SD$. Q. E. D.

PROP. XIII. FIG. 13.

If a body acted upon by any centripetal force, be any way moved, and another body descend or ascend in a right line, and their velocities be equal in any one case of equal altitudes, their velocities will be also equal at all equal altitudes.

Let a body descend from A, through D and E to the center C; and let another body move from V, in the curve VBK; from the center C, with any distances infinitely near to each other, describe the circles DB, EK; draw CB, meeting KE in N; on BK let fall the perpendicular NT; and imagine the bodies at D and B to have equal velocities: then, because the distances CD, CB, are equal, the centripetal forces in D and B will be equal. (Prop. VIII.) Let these forces be expressed by the equal lines DE, BN; and let the force BN be resolved into the forces NT and TB; the force NT will not affect the velocity of the body in the curve; but the other force BT will be employed in accelerating it. Because B and K, and likewise D and E, are indefinitely near to each other; the accelerating force from B to K, and from D to E, may be considered uniform; therefore the accelerations of the bodies in D and B, produced in equal times, are as the lines DE, BT;

Ther. $\text{vel. at E} : \text{vel. at T} :: DE (BN) : BT$;

But because BNK is a right angle, $BN = \sqrt{BT} \times \sqrt{BK}$;

Ther. $\text{vel. at E} : \text{vel. at T} :: \sqrt{BT} \times \sqrt{BK} : BT :: \sqrt{BK} : \sqrt{BT}$;

But, $\text{vel. at K} : \text{vel. at T} :: \sqrt{BK} : \sqrt{BT}$, (the spaces being as the squares of the velocities);

Ther. $\text{vel. at E} : \text{vel. at T} :: \text{vel. at K} : \text{vel. at T}$;

Therefore the velocity at E is equal to the velocity at K.
Q. E. D.

PROP. XIV. FIG. 14.

Let there be a semicircle whose diameter is AB , and center C ; bisect CB in D ; draw DE perpendicular to AB , and join AE . If from any point F in the semicircle there be drawn FG , perpendicular to AB , meeting AB in G , and AE in H , the DE^3 will be greater than $FG \times GH$.

Let EK , a tangent at E , meet AB in K , and FG in L , and join CE ; then by a property of the circle, $CK : CE :: CE : CD$, or $CK : CB :: CB : CD$; because $CB = 2CD \therefore CK = 2CB \therefore CB = BK = CA$;

And because $BD = DC \therefore AD = DK$.

And because $AD^3 : AD \times AG :: AD : AG :: DE : GH :: DE^3 : DE \times GH$;

Ther. $AD^3 : DE^3 :: AD \times AG : DE \times GH$.

Since $AG \times GK : AG \times DA :: GK : AD (DK) :: GL : DE :: GL \times GH : DE \times GH$; ther. $AG \times GK : LG \times GH :: AG \times AD : DE \times GH$;

Hence $AD^3 : DE^3 :: AG \times GK : LG \times GH$.

But AD^3 is greater than $AG \times GK$; ther. DE^3 is greater than $LG \times GH$; but GL is greater than GF , therefore DE^3 is greater than $FG \times GH$. Q. E. D.

PROP. XV. FIG. 15.

In the straight line AB , take BC , so that AC may be triple CB ; and let D be any point in AB ; the ratio of the cube of DA to the cube of AC will be less than the ratio of BC to BD .

Upon AB describe a semicircle AFB ; and let CF be perpendicular to AB ; join AF , and draw DG parallel to CF , meeting AF in H ; and let $KD \times DH = CF^2$.

Because $KD \times DH = CF^2$; $DH : CF :: CF : DK$;

But $DH : CF :: AD : AC :: CF : DK$;

Ther. $AD^3 : AC^3 :: CF^3 : DK^3 :: AD^3 : AC^3 \times AD$;

But, $AC^3 \times AD : AC^3 :: AD : AC :: AD \times CB : AC \times CB = CF^3$;

Ther. $AD^3 : AC^3 :: AD \times CB : DK^3$;

But (Prop. XIV.) CF^3 is greater than $GD \times DH$;

Therefore $KD \times DH$ is greater than $GD \times DH$;

Hence KD is greater than GD ; or KD^2 greater than GD^2 ;

But $GD^2 = AD \times DB$; ther. KD^2 is greater than $AD \times DB$;

Hence the ratio of $AD \times BC$ to $AD \times BD$, or of BC to BD , is less than the ratio of $AD \times BC$ to DK^2 ;

Ther. the ratio of AD^2 to AC^2 is less than the ratio of BC to BD .

PROP. XVI. FIG. 16.

Let A be a given point in the straight line AB ; and CDE a curve, such, that if from any two points C, D , there be drawn CF, DG , perpendicular to AB , so that $AG^2 : AF^2 :: CF : DG$, and that $AH = 4HF$, and CH be joined; then will CH be a tangent to the curve in the point C .

From any point K , in CH , draw KG perpendicular to AB , meeting AB in G , and the curve in D . Because $AH = 4HF$, $\therefore HF = \frac{1}{4}AH$; and $AH - HF = AF = AH - \frac{1}{4}AH = \frac{3}{4}AH$; ther. $AF : HF :: 3 : 1$. $\therefore AF = 3HF$; hence (Prop. XV.) $AG^2 : AF^2$ is less than $HF : HG$; but (hypoth.) $AG^2 : AF^2 :: CF : DG$; and $FH : HG :: FC : GK$, (by sim. triangles); therefore $CF : DG$ is less than $FC : GK$; therefore DG is greater than GK ; therefore, the point K is without the curve CDE . In the same way it is shewn, that any other point in CH is without the curve CDE ; therefore CH is a tangent to the curve CDE at the point C . Q. E. D.

PROP. XVII. FIG. 17.

Let A be a given point in the straight line AB , and CDE a curve, such, that if from any two points D, E , in the curve, there be drawn DF, EG , perpendicular to AB , $DF : EG :: AG^2 : AF^2$;—also draw AH perpendicular, and DK, EL , parallel to AB ; then will the space $DKLE = 3 \times DFGE$, and $AF \times FD - AG \times GE = 2 \times DFGE$.

Suppose KL to be divided into indefinitely little parts in M, N , &c.; draw MO, NP , &c. parallel, and OV, PX , &c. perpendicular to AB ; let DF, OV, PX , meet MO, NP, LE , in

q, r, s ; and let T be a point in AB , such, that $AT=4FT$, and join DT .

Because (Prop. XVI.) $AG^2 : AF^2 :: DF : EG$, and $AT=4FT$; DT will be a tangent to the curve at D ; and because MO is indefinitely near to DK , the triangles DFT, DqO , may be considered as similar; ther. $DF : FT :: Dq : qO$, $\therefore FT \times Dq = DF \times qO = FO$; but because $AT=4FT, AF=3FT$ $\therefore AF \times Dq = 3FT \times Dq \therefore DM = 3FO$. The same way it may be shewn that $ON=3VP, PL=3EX$, &c. But $DM + ON + PL + \&c. = DKLE$, and $FO + VP + EX + \&c. = DFGE$; ther. $3FO + 3VP + 3EX + \&c. = DKLE$, therefore the space $DKLE = 3 \times DFGE$.

Again let DF meet EL in Y , because $DKLE = 3 \times DFGE$ $\therefore DL + DYE = 3DYE + 3FE$, or $DL = 3FE + 2DYE = FE + 2FE + 2DYE = FE + 2 \times DFGE$; add LF to both sides of the equation, then $DL + LF = FE + 2 \times DFGE + LF$ $\therefore AD = AE + 2 \times DFGE$, ther. $AF \times FD - AG \times GE = 2 \times DFGE$. Q.E.D.

PROP. XVIII. FIG. 18.

Let S be a given point in the straight line AS , and CDE a curve, such, that if from any two points A, B , there be drawn AC, BD , perpendicular to AS ,

$BD : AC :: AS^2 : SB^2$; and let $SA=SF$. Then,
 $SA \times AC : CABD :: 2SB^2 : AB \times BF$; likewise,
 $SB \times BD : CABD :: 2SA^2 : AB \times BF$.

Let $AS^2 \times SG = SB^2 \therefore AS^2 : SB^2 :: SB : SG$;

Because $BD : AC :: AS^2 : SB^2 (AS^2 \times SG) :: AS : SG$;

Ther. $AC \times AS = SG \times BD$;

Hence $SB \times BD : SA \times AC :: SB \times BD : SG \times BD :: SB : SG :: AS^2 : SB^2$. Ther. $AS^2 - SB^2 : SB^2 :: SB \times BD - SA \times AC : SA \times AC$.

That is, $FB \times AB : SB^2 :: SB \times BD - SA \times AC : SA \times AC$;

But (Prop. XVII.) $SB \times BD - SA \times AC = 2 \times CABD$,

Ther. $FB \times AB : SB^2 :: 2 \times CABD : SA \times AC$,

Or $FB \times AB : 2SB^2 :: 2CABD : 2SA \times AC : 2CABD : SA \times AC$.

Again, because $SB \times BD : SA \times AC :: AS^2 : SB^2 :: 2AS^2 : 2SB^2$;

And - - $SA \times AC : CABD :: 2SB^2 : FB \times AB$,

Therefore $SB \times BD : CABD :: 2SA^2 : FB \times AB$. Q.E.D.

PROP. XIX. FIG. 19.

The law of centripetal force being given, and the quadrature of curves being granted, it is required to find the trajectory in which a body will move, that sets out from a given place, with a given velocity, in the direction of a given right line.

Suppose $A EFG$ to be the trajectory: with the center C , and distance CA , describe the circle APQ ; draw AY , CZ , perpendicular to CA ; with the asymptotes CA , CZ , let there be an hyperbola described passing through the point Y ; let SRT be a curve, such, that drawing any line CFP , meeting the trajectory in F , and the circle in P , and with the center C , and distance CF , a circle be described meeting CA in K , and KR be drawn perpendicular to CA , meeting the curve in R , the space $SAKR$ will be double the sector ACP : Let fall CB perpendicular to AB , the given right line in which the body is projected; let AE , FG , be indefinitely little parts of the trajectory described in equal times; with the center C , and distances CE , CF , CG , describe the circles EH , FK , GL ; and let the circle GL meet CF in M ; let DA be the space through which the body would fall, so as to acquire, at the point A , a velocity equal to that with which the body is projected in the direction AB ; let CX be to CK as the velocity that would be acquired in falling from D to K , to the velocity that would be acquired in falling from D to A ; draw La parallel to KR , meeting the curve in a ; join CG , and let it meet the circle APQ in Q ; and let KR meet the hyperbola in V .

Because the body sets out at A , to describe the trajectory with the velocity acquired in falling from D to A , and CF is equal to

CK, the velocity at F will be equal (Prop. XIII.) to the velocity acquired in falling from D to K;

Ther. (hypoth.) vel. at A : vel. at F :: CK : CX :: AE : FG;

But because AE, FG, are described in equal times, the triangles CAE, CFG are equal; ther. $AE \times CB = CF \times GM = CK \times GM$. $\therefore CB : CK :: GM : AE :: CX : FG$,

Ther. $CB^2 : CX^2 :: GM^2 : FG^2$. $\therefore CX^2 - CB^2 : CB^2 :: FG^2 - GM^2 : GM^2 :: FM^2 : GM^2$.

Again, because from the nature of the curve, SRT, the space $SAL = 2 \times \text{sector CAQ}$, and $SAKR = 2 \times \text{sector CAP}$, ther. $RKL = 2 \times \text{sector CPQ}$; and because KL is indefinitely little, $KR \times KL = CP \times PQ$,

Ther. $KL : PQ :: CP : KR : CA : KR$;

But $PQ : GM :: CP : CM = CL = CK :: CA : CK :: KV : AY = CA$;

Ther. $KL : GM :: KV : KR :: FM : GM$;

Hence, $KV^2 : KR^2 :: FM^2 : GM^2 :: CX^2 - CB^2 : CB^2$; ther. KR is given.

From whence may be deduced the following

CONSTRUCTION.

Draw AY, CZ, perpendicular to CA, and let AY be equal to CA; with the asymptotes CA, CZ, let there be an hyperbola described passing through the point Y; and let the body set out from A in the direction of the right line AB, with the velocity acquired in falling from D to A; draw CB perpendicular to AB; and let K be any point in AC; let CX be to CK, as the velocity that would be acquired in falling from D to K, to the velocity that would be acquired in falling from D to A; let SRT be a curve, such, that drawing KV perpendicular to AC, meeting the hyperbola in V, and the curve SRT in R, $KV^2 : KR^2 :: CX^2 - CB^2 : CB^2$; let AY meet the curve SRT in S;—with the center C, and distance CA, describe the circle APQ; draw CP, such, that the area SAKR may be double the sector CAP; and with the center C, and distance CK, describe a circle meeting CP in F: F will be a point in the trajectory. Q. E. I.

PROP. XX. FIG. 20.

Suppose a body, acted upon by a centripetal force tending to the center S , to descend in the right line AS ; let there be a curve CDE , such, that if from any two points A, B , in AS , there be drawn AC, BC , perpendicular to AS , the centrip. force at A : centrip. force at B :: $AC : BE$. Suppose the body at the point B to be projected in the direction BF , perpendicular to SB , with the velocity that would be acquired in falling from A to B ; and let the centrifugal force at the point B , arising from the projectile force, be greater than the centripetal force at B : It is evident that the body will recede from the center S : In SA take SG , equal to the greatest distance the body will recede from the center : The sum of the centrifugal forces that have acted upon the body while it receded from the center, through the space BG , will be equal to the sum of the centripetal forces that have acted upon the body in the same time.

Let $SB \times BF = 2 \times C A B E$; in BE take BH , so that $BH^2 = C A B E$; draw SK perpendicular to SB ; with the asymptotes SB, SK , describe an hyperbola to pass through the point H ; let BLM be the trajectory described by the body; suppose the body at the point L in the trajectory; and let LM, BO , be described in indefinitely little equal parts of time; join SL, SM, SO ; with the center S , and distance SL , describe the arc LG meeting SA in G ; and with the center S , and distance SM , describe the arc MN meeting SL in N ; draw GD perpendicular to SA , meeting the curve CDE in D , and the hyperbola in P .

Because BO, LM , are described in equal times, and the velocity in a circle equable,

$LM : BO :: \text{vel. at } L : \text{vel. at } B :: \text{vel. at } G : \text{vel. at } B :: \sqrt{CAGD} : \sqrt{CABE}$ (Hypoth. and Prop. III.);

Ther. $LM^2 : BO^2 :: CAGD : CABE :: CAGD : BH^2$ (hypoth.); and because the triangles SLM, SBO , are equal, $BO^2 : MN^2 :: SL^2 (SG^2) : SB^2 :: BH^2 : GP^2$ (proport. of hyperbola); ther. $LM^2 : MN^2 :: CAGD : GP^2$. Hence it is

evident, that when $LM = MN$, $CAGD = GP^2$; and therefore $SL = SG$, will be the greatest distance the body will recede from the center S .

Let there be a curve FQ , so related to SA , that if from any two points B, G , there be drawn BF, GQ , perpendicular to SA , the $SG^2 : SB^2 :: BF : GQ$; produce GS to R , and let $SR = SG$.

But (Prop. XI.) centrif. force at B : centrip. force at $B :: 2 \times C A B E : SB \times BE :: SB \times BF : SB \times BE :: BF : BE$ (because $SB \times BF = 2 \times C A B E$); therefore, because BE represents the centripetal force at B , BF will represent the centrifugal force at B ; but (Prop. VIII.) the centrifugal forces are reciprocally as the cubes of the distances from the center: therefore it is evident, that while the body receded from the center through the space BG ;

The sum centrif. forces : sum centrip. forces :: $FBGQ : EBGD$;

And because $BH^2 = C A B E$, $GP^2 = C A D G$;

Ther. $C A B E : C A D G :: BH^2 : GP^2 :: SG^2 : SB^2$ (hyperbola);

Ther. $C A B E : EBGD :: SG^2 : SG^2 - SB^2 = BR \times BG$;

Ther. $SB \times BF : EBGD :: 2SG^2 : BR \times BG$; but (Prop. XVII.) $SB \times BF : FBGQ :: 2SG^2 : BR \times BG$;

Ther. $SB \times BF : FBGQ :: SB \times BF : EBGD$, $\therefore FBGQ = EBGD$;

Therefore the sum of the centrifugal forces that have acted upon the body while it receded from the center, through the space BG , will be equal to the sum of the centripetal forces that have acted upon the body in the same time.

COROLLARY.

From this it is evident, that the sum of the centrifugal forces that act upon a body while it revolves from apsis to apsis, is equal to the sum of the centripetal forces that act upon it in the same time.

PROP. XXI. FIG. 21.

Let there be an ellipse whose transverse axis is AB , and foci D, E ; produce DA to F ; and let DF be equal to AB ; upon DF let a semicircle be described; draw DG, DH , to any two points in the ellipse; and draw DK, DL , perpendicular to GK, HL , tangents to the ellipse at G and H ; with the center D , and distances DG, DH , describe the circles GM, HN ; draw MO, NP , perpendicular to AD ; and join DO , meeting NP in Q ; then will $DK : DL :: NP : NQ$.

Join EG ; and draw ER perpendicular to the tangent GK . Because $DG + GE = AB = DF$, and $DG = DM$; ther. $DM + GE = DF$. $\therefore GE = DF - DM = FM$; ther. $DM : FM :: DG : GE$; but $DM \times MF = MO^2$. $\therefore DM^2 : MO^2 :: DM : MF :: DG : GE$; because KR is a tangent at G , the angles DGK, EGR , will be equal; and the angles at K and R being right, the triangles DGK, EGR , are equiangular; ther. $DK : ER :: DG : GE :: DK^2 : DK \times ER :: DM^2 : MO^2$, but (26 Ellip.) $DK \times ER = AD \times DB$; ther. $DK^2 : AD \times DB :: DM^2 : MO^2$.

In the same way it is shewn that $DL^2 : AD \times DB :: DN^2 : NP^2$;

Ther. $AD \times DB : DL^2 :: NP^2 : DN^2$;

But $DK^2 : AD \times DB :: DM^2 : MO^2 :: DN^2 : NQ^2$;

Ther. $DK^2 : DL^2 :: NP^2 : NQ^2$; or, $DK : DL :: NP : NQ$. Q. E. D.

COROLLARY. $DK^2 : AD \times DB :: DG : GE$.

PROP. XXII. FIG. 22.

Let there be a semicircle whose diameter is AB ; and let ADE be a curve, such, that if from any two points D, E , there be drawn DC, EF , perpendicular to AB , meeting the semicircle in G, H , and joining BG , meeting FH in K , $EF : DC :: FH^2 : FK^2$, the curve ADE , will be an hyperbola: and let DL, EM be tangents at D, E ; $EF \times CL : DC \times FM :: BC^2 : BF^2$.

Bisect AB in C ; produce EF , so that $FO=DC$; through O , draw PN parallel to AB , meeting AN , BP , perpendicular to AB , in N , P ; and DC in R .

Because $EF : DC :: FH^2 : FK^2$; and $FH^2 = AF \times FB$, and $FK^2 = FB^2$ (because $CG = CB$) therefore, $EF : DC (FO) :: AF \times FB : FB^2 :: AF : FB$;

Hence $EF + FO : FO :: AF + FB : FB$;

That is, $EO : FO (AN) :: AB : FB :: NP : PO \therefore EO \times PO = AN \times NP$;

Therefore the curve ADE is an hyperbola whose asymptotes are PB and PN .

Again, let DC , and the tangents DL , EM , meet PN in R , N , Q . Because a tangent drawn at any point in an hyperbola to meet the asymptotes is bisected in the point of contact; $NR = RP$, and $QO = OP$; and because $EF : FM :: EO : OQ (OP) :: EF \times LC : FM \times LC :: EO^2 : OP \times EO$. Again, because $LC : CD :: NR : RD :: PR : RD :: LC \times FM : CD \times FM :: PR \times RD : RD^2 :: EO \times OP : RD^2$ (prop. of hyperbola); but $EF \times LC : FM \times LC :: EO^2 : OP \times EO$; ther. $EF \times LC : CD \times FM :: EO^2 : RD^2$; because $EO \times OP = DR \times RP$, $EO : DR :: RP : OP :: CB : BF \therefore EO^2 : DR^2 :: CB^2 : BF^2 :: EF \times LC : CD \times FM$. Q. E. D.

PROP. XXIII. FIG. 22.

Suppose a body to descend or ascend in the line AB ; let C , F , be any two points in AB ; draw CG , FH , perpendicular to AB , meeting the semicircle described upon AB in G , H ; join BG meeting FH in K . If the vel. at F : vel. at $C :: FH : FK$, then will the centrip. force at F : centrip. force at $C :: BC^2 : BF^2$.

Let ADE be a curve, such, that if from any two points D , E , there be drawn DC , EF , perpendicular to AB , meeting the semicircle in G , H , and joining BG , meeting FH in K ; $EF : CD :: HF^2 : FK^2$; and let DL and EM be tangents to the curve at D , E .

Because $HF^2 : FK^2 :: EF : CD \therefore HF : FK :: \sqrt{EF} :$

$\sqrt{CD}$; but, vel. at F : vel. at C :: HF : FK :: $\sqrt{EF}$: $\sqrt{CD}$;
 ther. (Prop. V.) centrip. force at F : centrip. force at C :: $EF \times$
 $CL : DC \times FM :: BC^2 : BF^2$ (Prop. XXII.) Q. E. D.

PROP. XXIV. FIG. 21.

If a body revolve in an ellipse, and be acted upon by a centripetal force tending to the focus of the ellipse, the centripetal force will be reciprocally as the square of the distance from the focus.

Let a body revolve in the ellipse whose transverse axis is AB, and be acted upon by a centripetal force tending to the focus D; produce DA, so that $DF = AB$; draw DG, DH, to any two points in the ellipse; draw DK, DL, perpendicular to the tangents at G and H; with the center D, and distances DG, DH, describe the circles GM, HN; draw MO, NP, perpendicular to AD, meeting the semicircle described upon DF in O, P; join DO meeting NP in Q.

Suppose a body to descend or ascend in the line AD, and at the point A to have acquired a velocity equal to the velocity which the body describing the ellipse has at the point A; the velocities of the bodies at G and M will be equal (Prop. XIII.); and likewise the velocities of the bodies at H and N will be equal: but (Prop. XII.) vel. at H : vel. at G :: DK : DL :: NP : NQ. (Prop. XXI.)

Ther. vel. at N : vel. at M :: NP : NQ;

Ther. (Prop. XXIII.) centrip. force at N : centrip. force at M :: $DM^2 : DN^2 :: DG^2 : DH^2$; because $DG = DM$, $DH = DN$, and GM, HN, circles; the centrip. force at G is equal to the centrip. force at M; and the centrip. force at H equal to the centrip. at N;

Ther. centrip. force at H : centrip. force at G :: $DG^2 : DH^2 ::$

$$\frac{1}{DH^2} : \frac{1}{DG^2}.$$

OTHERWISE, FIG. 23.

Let S be the focus of the ellipse, AB the greater axis, C the center, CD half the less axis; suppose a body in indefinitely

little equal parts of time to describe AE , FG ; join SE , SF , SG ; draw EK perpendicular to AB , and GM perpendicular to SF ; let FP be a tangent at F ; draw GP parallel to SF ; join CF meeting the ellipse in H ; and let GN , drawn parallel to FP , meet SF , CF , in N , O ; draw CQ parallel to FP meeting SF in V ; complete the parallelogram $FCQT$; and draw FR perpendicular to CQ .

Because QV , GN are parallel, and the angles at M and R , right, the triangles FRV , GMN are similar; ther. $MG : GN :: RF : FV = CA$ (ellip. 25. cor.) : but (ellip. 31. cor. 2.) $RF \times CQ = CA \times CD$; ther. $RF : CA :: CD : CQ :: MG : GN$; but GN , GO may be considered as equal, because FG is described in an indefinitely little part of time; ther. $MG^2 : GO^2 :: CD^2 : CQ^2$; but (ellip. 16.) $GO^2 : HO \times OF :: CQ^2 : CF^2$ $\therefore MG^2 : HO \times OF :: CD^2 : CF^2$; but $HO \times OF$, may be considered equal to $HF \times FO$; ther. $GM^2 : HF \times FO :: CD^2 : CF^2$; but $HF \times FO : HF \times FN :: FO : FN :: FC : FV$ (CA) $:: CF^2 : CA \times FC \therefore GM^2 : HF \times FN :: CD^2 : CA \times CF$;

But $HF \times FN : AB \times FN :: HF : AB :: CF : CA :: FC \times CA : CA^2$;

Ther. $GM^2 : AB \times FN :: CD^2 : CA^2 :: EK^2 : AK \times KB$ (ellip. 3.)

But $BK \times KA$, may be considered equal to $BA \times AK$;

Ther. $GM^2 : AB \times FN :: EK^2 : BA \times AK$;

That is, $GM^2 : EK^2 :: AB \times FN : AB \times AK :: FN : AK$;

But because AE , FG , are described in equal times the triangle $SAE = SFG$; that is, $SA \times EK = SF \times GM$; $\therefore GM^2 : EK^2 :: SA^2 : SF^2$;

Ther. FN (GP) : $AK :: SA^2 : SF^2$; that is, $GP : KA :: \frac{1}{SF^2} : \frac{1}{SA^2}$.

Therefore the centripetal force is reciprocally as the square of the distance from the focus. Q. E. D.

PROP. XXV. FIG. 24.

If a body revolve in an ellipse, it is required to find the law of centripetal force tending to the center of the ellipse.

Let AB be the greater axis, C the center, and CD half the lesser axis; and suppose a body in indefinitely little equal parts of time to describe AE, FG; join CF, CE, CG; draw EK perpendicular to AB, and GM perpendicular to CF; let FP be a tangent at F; draw GP parallel to CF, and GN, CQ parallel to FP; complete the parallelogram FCQT; draw FR perpendicular to CQ, and let CF meet the ellipse in H.

Because the parts AE, FG, are described in equal times, $CA \times EK = CF \times GM$, $\therefore EK^2 : GM^2 :: CF^2 : CA^2$; because GN is parallel to CQ, and the angles at M and R are right, the triangles GNM, FCR, are equiangular;

Ther. $GM^2 : GN^2 :: FR^2 : FC^2 \therefore EK^2 : GN^2 :: FR^2 : CA^2 :: CD^2 : CQ^2$ (ellip. 31. cor. 2.); but (ellip 16.) $GN^2 : HN \times NF :: CQ^2 : CF^2$;

Ther. $EK^2 : HN \times NF :: CD^2 : CF^2 \therefore HN \times NF : EK^2 :: CF^2 : CD^2$;

But (ellip. 3.) $EK^2 : BK \times KA :: CD^2 : CA^2 \therefore HN \times NF : BK \times KA :: CF^2 : CA^2$;

But because AE, FG, are indefinitely little, we may consider $HN \times NF = HF \times FN$, and $BK \times KA = BA \times AK$;

Ther. $HF \times FN : BA \times AK :: CF^2 : CA^2 :: CF \times FN :: CA \times AK$;

Ther. $FN(GP) : AK :: CF : CA$;

But $GP : AK ::$ centrip. force at F : centrip. force at A :: $CF : CA$.

Therefore the centripetal force tending to the center of the ellipse is as the distance from the center of the ellipse. Q.E.I.

PROP. XXVI. FIG. 25.

Let there be an ellipse whose transverse axis is AB; in which let F be a given point; suppose a body acted upon by a centripetal force, tending to the point F, to describe the ellipse: it is required to determine the law of centripetal force tending to the point F.

Let C be the center of the ellipse, and E the focus; and let CD be half the less axis; let KL, AG, be described in indefinitely little equal parts of time; join FK, CK, EK, and FL; draw LP perpendicular to FK; draw LM parallel to FK, meeting the tangent KM in M; draw LN parallel to KM, meeting FK, CK, in N, O; draw CQ parallel to KM, meeting FK, EK, in Q, X; and draw FY parallel to CQ or KM; let CK, CQ, meet the ellipse in T, R; and draw KS perpendicular to CR, meeting FY in Z; draw GH perpendicular to AB; join FG; and let $CA \times KY = AF \times FV$.

Because LN, FZ, are parallel, and the angles at P and Z right; the triangles LPN, FKZ, are similar; ther. $NL : LP :: FK : KZ$. $\therefore NL \times KZ = LP \times FK$; and because KL, AG, are described in equal times, ther. $LP \times FK = GH \times FA = NL \times KZ$. $\therefore LN : GH :: AF : KZ :: AF \times CR : KZ \times CR$; but $KZ : KY :: KS : KX(CA) :: CD : CR$;

Ther. $KZ \times CR = CD \times KY$. $\therefore LN : GH :: AF \times CR : CD \times KY$;

Ther. $LN^2 : GH^2 :: AF^2 \times CR^2 : CD^2 \times KY^2$;

But $GH^2 : BH \times HA :: CD^2 : CA^2 :: CD^2 \times KY^2 : CA^2 \times KY^2$;

Ther. $LN^2 : BH \times HA :: AF^2 \times CR^2 : CA^2 \times KY^2 = AF^2 \times FV^2$ (hypoth.);

Ther. $LN^2 : BH \times HA :: CR^2 : FV^2$;

But because KL is indefinitely little, we may consider $LN = LO$, ther. $BH \times HA : LO^2 :: FV^2 : CR^2$;

But $LO^2 : TO \times OK :: CR^2 : CK^2$. $\therefore BH \times HA : TO \times OK :: FV^2 : CK^2$;

But because AG, KL, are indefinitely little, we may consider $BH \times HA = BA \times AH$, and $TO \times OK = TK \times KO$;

Ther. $BA \times AH : TK \times KO :: FV^2 : CK^2$;

But $TK \times KO : TK \times KN :: KO : KN :: KC : KQ :: KC^2 : KQ \times KC$, ther. $BA \times AH : TK \times KN :: FV^2 : CK \times KQ$;

But $TK \times KN : AB \times KN :: CK : CA :: CK \times KQ : CA \times KQ$;

Ther. $BA \times AH : AB \times KN :: FV^2 : CA \times KQ$;

Ther. $AH : KN :: FV^3 : AC \times KQ$.

Because $CA \times KY = AF \times FV \therefore FV^3 : CA^3 :: KY^3 : AF^3 :: KY^3 \times FK : AF^3 \times FK$; but $CA^3 : CA \times KQ :: AC : KQ :: KX : KQ :: KY : KF :: KY^3 : KY^3 \times KF$; ther. $FV^3 : CA \times KQ :: KY^3 : AF^3 \times FK$; ther. $AH : KN :: KY^3 : AF^3 \times FK$; but because GH is parallel to the tangent at A , and LN parallel to the tangent at K ; and AG , LK , are indefinitely little, and described in equal times.

The centrip. force at A : centrip. force at $K :: AH : KN :: KY^3 : AF^3 \times KF$. Q. E. D.

COROLLARY. This proposition comprehends the two former ones; for if the point F coincide with the focus E , the point Y will coincide with E ; and $KY^3 = KE^3$; likewise $AF^3 \times KF = AE^3 \times KE \therefore AH : KN :: KE^3 : AE^3 \times KE :: KE^3 : AE^3$; which agrees with Prop. XXIV.

When F coincides with C , $KY = KX = CA$;

$AF = AC$, and $FK = CK$; therefore

$AH : KN :: CA^3 : CA^3 \times CK :: CA : CK$; which agrees with Prop. XXV.

PROP. XXVII. FIG. 26.

If a body describe an hyperbola, it is required to find the law of centripetal force tending to the focus.

Let S be the focus of the hyperbola, AB the transverse axis, C the center, and CD half the second axis; let AE , FG , be described in indefinitely little equal parts of time; join SE , SF , SG ; draw EK perpendicular to SA , and GM perpendicular to SF ; let FP be a tangent at F ; draw GP parallel to SF ; join CF , which produce, so that $CF = CH$; let GN , drawn parallel to FP , meet SF , CF , in N , O ; let CQ , the semi-diameter conjugate to CF , meet SF in V ; complete the parallelogram $FCQT$; and draw FR perpendicular to CQ .

Because QV , GN , are parallel, and the angles at R and M right; the triangles FRV , GMN , will be similar; ther. $GM : GN :: FR : FV = CA$; but the parallelogram $FCQT = CQ \times FR = AC \times CD$, $\therefore FR : CA :: CD : CQ :: GM : GN$; but

because FG is described in an indefinitely little part of time, we may consider $GN = GO$; ther. $GM^2 : GO^2 :: CD^2 : CQ^2$; but $GO^2 : HO \times OF :: CQ^2 : CF^2$; ther. $GM^2 : HO \times OF :: CD^2 : CF^2$; we may consider $HO \times OF = HF \times OF$; therefore, $GM^2 : HF \times OF :: CD^2 : CF^2$; but $HF \times FO : HF \times FN :: FO : FN :: CF : FV(CA) :: CF^2 : FC \times CA$; ther. $GM^2 : HF \times FN :: CD^2 : FC \times CA$; but $HF \times FN : AB \times FN :: HF : AB :: CF : CA :: CF \times CA : CA^2$; ther. $GM^2 : AB \times FN :: CD^2 : CA^2 :: EK^2 : BK \times KA$; but we may consider $BK \times KA = BA \times AK$; therefore, $GM^2 : AB \times FN :: EK^2 : BA \times AK$; that is, $GM^2 : EK^2 :: FN : AK$; but because AE, FG , are described in equal times, $SA \times EK = SF \times GM$; therefore $GM^2 : EK^2 :: SA^2 : SF^2 :: FN : AK :: GP : AK$;

Hence the centrip. force at F : centrip. force at $A :: GP : AK :: SA^2 : SF^2 :: \frac{1}{SF^2} : \frac{1}{SA^2}$; therefore the centripetal force is reciprocally as the square of the distance from the focus S . $Q. E. I.$

PROP. XXVIII. FIG. 27.

If a body describe a parabola, it is required to find the law of the centripetal force tending to the focus of the parabola.

Let S be the focus of the parabola, AB the axis, and A the vertex; let AE, FG , be described in indefinitely little equal parts of time; join SE, SF, SG ; draw EK perpendicular to SA , and GM perpendicular to SF ; let FP , a tangent at F , meet SA in R ; draw FC parallel to AB , and GP parallel to SF , and GN parallel to FP , meeting SF, FC , in N, O ; and draw SQ perpendicular to FR .

Because GN, FQ , are parallel, and the angles at M and Q right; the triangles GNM, SFQ , are similar; ther. $NG : GM :: SF : SQ$; because FG is described in an indefinitely little part of time, we may consider $GN = GO$; ther. $OG^2 : GM^2 :: SF^2 : SQ^2 :: SF^2 : SA \times SF :: SF : SA$ (Prop. of Parabola.)

Again, because $GO^2 = FO \times (\text{Param. of } CF) = FO \times 4SF$;

ther. $4 \times SF \times FO : GM^2 :: SF : SA :: 4SF \times FO : 4SA \times FO$; ther. $GM^2 = 4SA \times FO$; but $EK^2 = 4SA \times AK$; ther. $GM^2 : EK^2 :: FO : AK$; but because NO is parallel to FR , and FO parallel to SR , the triangles FNO , FSR , are similar; ther. $NF : FO :: FS : SR$; but $SF = SR$, ther. $FN = FO \therefore GM^2 : EK^2 :: FN : AK$; because AE , FG , are described in equal times, therefore $SA \times EK = SF \times GM \therefore GM^2 : EK^2 :: SA^2 : SF^2 :: FN : AK$; but because $FN = GP$; $SA^2 : SF^2 :: GP : AK :: \frac{1}{SF^2} : \frac{1}{SA^2}$; therefore the centripetal force is reciprocally as the square of the distance from the focus S . Q.E.I.



ADDENDA.

COROLLARIES TO PROP. XLIV. OF THE ELLIPSE.

COROLLARY 1.

FROM hence it appears, that the conjugate diameter KW produced, is the *locus* of the centers of curvature of every degree that is perpendicular to, and bisected by, the meridian IKHW.

COROLLARY 2.

When the angle $PXH = 45^\circ$, then $t=1$, and the secant $= \sqrt{2}$; we then have $vs = \frac{2 \cdot CH^2 \cdot CK}{CH^2 + CK^2}$, $vP = \frac{2\sqrt{2} \cdot CH^2 \cdot CK^2}{(CH^2 + CK^2)^{\frac{3}{2}}}$, and the radius of curvature of a degree perpendicular to the meridian in lat. $45^\circ = \frac{\sqrt{2} \cdot CH^2}{(CH^2 + CK^2)^{\frac{3}{2}}}$.

COROLLARY 3.

When P coincides with K, the angle $PXH = 90^\circ$, and both the tangent and secant become infinite in length.

$$\text{Then } vs = \frac{CH^2 \cdot CK \cdot (\text{inf.})^2}{\sqrt{(\text{inf.})^2 \cdot CK^2} \times \sqrt{(\text{inf.})^2 \cdot CH^2}} = CH.$$

$$vP = \frac{CH^2 \cdot CK^2 \cdot (\text{inf.})^3}{(\text{inf.})^2 \cdot CH^2 \cdot \sqrt{(\text{inf.})^2 \cdot CK^2}} = CK, \text{ and half the}$$

$$\text{latus-rectum of } PZ = \frac{CH^2 \cdot \text{inf.}}{\sqrt{(\text{inf.})^2 \cdot CK^2}} = \frac{CH^2}{CK}.$$

COROLLARY 4.

When P coincides with H, the angle PXH is nothing, its secant unity, and $t=0$; then

$$vs = \frac{CH^2 \cdot CK}{\sqrt{CH^2} \cdot \sqrt{CK^2}} = CH, \quad vP = \frac{CH^2 \cdot CK^2}{CK^2 \cdot \sqrt{CH^2}} = CH,$$

and half the latus-rectum of PZ = $\frac{CH^2}{\sqrt{CH^2}} = CH$. In this case the section PtZs, evidently becomes a circle.

COROLLARY 5.

When the section IKHW is a circle, or $CH = CK$;

$$\text{Then } vs = \frac{(1+t^2) CH^2}{\sqrt{(1+t^2) CH^2} \times \sqrt{(1+t^2) CH^2}} = CH,$$

$$vP = \frac{(1+t^2) (1+t^2)^{\frac{1}{2}} \cdot CH^4}{(1+t^2) CH^2 \sqrt{(1+t^2) CH^2}} = CH, \text{ and half the}$$

$$\text{latus-rectum of PZ} = \frac{(1+t^2)^{\frac{1}{2}} \cdot CH^2}{\sqrt{(1+t^2) CH^2}} = CH.$$

PROPOSITION A.

The length of a degree perpendicular to a meridian, is greater than a corresponding meridional degree.

By Prop. XLIV. of the Ellipse, the radius of curvature of a degree perpendicular to the meridian in any given latitude is

$$\frac{CH^2}{c(CH^2 + t^2 \cdot CK^2)^{\frac{1}{2}}} = R,$$

And by Cor. 1. page 61, the radius of curvature of a meridional degree in any given latitude is $\frac{CH^2 \cdot CK^2}{\left\{ c(CH^2 + t^2 \cdot CK^2)^{\frac{1}{2}} \right\}^3} = P \odot$,

$$\text{from whence } R : P \odot :: 1 : \frac{CK^2}{c^2(CH^2 + t^2 \cdot CK^2)} :: \frac{CH^2}{CK^2} + t^2 : \frac{1}{c^2} :: \frac{CH^2}{CK^2} + t^2 : 1 + t^2.$$

Therefore, in any given latitude, the length of a degree perpendicular to the meridian is greater than the length of a corresponding meridional degree; the lengths of the degrees being as the radii of curvature and $\frac{CH^2}{CK^2}$ greater than unity.

COROLLARY 1.

Since $D' : D :: \frac{CH^2}{CK^2} + t^2 : 1 + t^2$, we get $\frac{CH^2}{CK^2} = \frac{D + (D' - D)t^2}{D}$.

Hence the ratio of the axes are known.

D' representing the length of a degree perpendicular to the meridian, and D the length of a corresponding meridional degree.

COROLLARY 2.

At the equator, $t=0$, and $D' : D :: \frac{CH^2}{CK^2} : 1 :: CH^2 : CK^2$.

COROLLARY 3.

In lat. 45° , $t=1$, and $D' : D :: \frac{CH^2}{CK^2} + 1 : 2$.

COROLLARY 4.

At the poles, $t = \text{tang. } 90^\circ$, and therefore infinitely long; then $D' : D :: \frac{CH^2}{CK^2} + (\text{inf.})^2 : 1 + (\text{inf.})^2 :: (\text{inf.})^2 : (\text{inf.})^2 \therefore D' = D$.

PROPOSITION B.

Having the meridional degree, and also the degree perpendicular to the meridian in a given latitude, to find the earth's axes, supposing it an ellipsoid. See Prop. XVI. page 66.

By Cor. 1. Prop. A. we have - - - $\frac{CK^2}{CH} = \frac{CH}{1 + mt^2}$ - - (a).

And from Prop. IV. page 57 - - - $\frac{CK^2}{CH} = v D \cos.^3 P f T$;

From whence $CH = vD(1 + m^2)^{-\frac{1}{2}} \cos. \angle P f T$ (fig. page 65, $y = 57.2957795$, and $\frac{D' - D}{D} = m$). From equation (a) $CH : \sqrt{CH^2 - CK^2} :: \sqrt{1 + m^2} : t\sqrt{m}$, and per trigonometry $\sqrt{1 + m^2} : t\sqrt{m} :: s : \frac{st\sqrt{m}}{\sqrt{1 + m^2}} = \sin. \angle P f T$, therefore $\left(\frac{1 + ms^2}{1 + m^2}\right)^{\frac{1}{2}} = \cos. \angle P f T$ ($s = \sin. t = \tan. \angle E f H$). By substitution, $CH^2 = \frac{v^2 D^2 (1 + ms^2)^2}{1 + m^2}$, and $CK^2 = \frac{v^2 D^2 (1 + ms^2)^2}{(1 + m^2)^2}$.

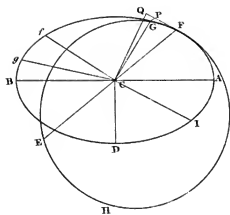
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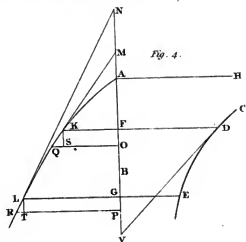
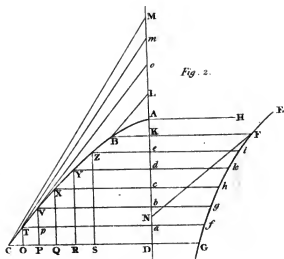
ERRATA.

Page.	Line.	Error.	Correction.
9	7	Ff	F, f
10	4	GH : CH	CH :: CH
14	9	QF ²	QF ²
17	---	Lemma 1.	Lemma
26	4	Pd×CG=CW ²	Pd×CG=CW ²
29	4	CRCK	CK
32	2	CE ² , EE ² -CG ² +CE ² -CE ²	CE ² -CG ² +CE ² -CE ²
36	15	sin. ² EDP=P D ²	sin. ² EDP×P D ²
38	15	CL : CW : gm : gr	CL : CW :: gm : gr
41	last	Fr-	Fr=
43	19	CF×cos. RFH	CF×cos. RfH
46	7	Common section PZ	normal PX
46	Fig.	k	h, and join PC
48	2		dele 1 in denominator
48	4	vortex	vertex
49	4	TPf	TPF
49	5	cor. 8	cor. 1
49	Fig.		P is omitted
50	7	Lemma 2.	Lemma
51	5	ther.	then
52	last	Add to the last line	(see Fig. to Prop. IV.)
63	last	(a ² -v ² S ²) ¹	(a ² -v ² S ²) ¹
90	14	Prop. XXXVII.	Prop. XXXVII. ellipse
99	23		dele A·C
106	21	vel. at F : vel. at F	vel. at F : vel. at f
110	1	a b ² :: d n ²	a b ² ×d n ²
113	9	GL ² : gl ²	GL ² : gl ²
123	6	SL : SL	SL : SI
		FG	F, G

Fig. 2.









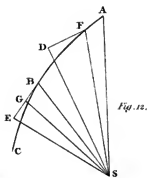
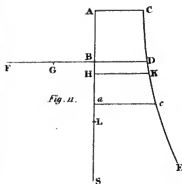
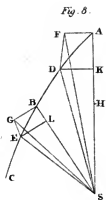
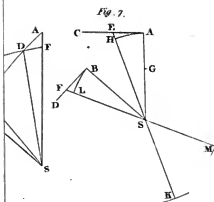


Fig. 15.

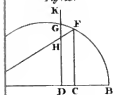


Fig. 16.

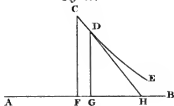


Fig. 19.

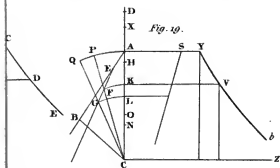


Fig. 22.

